

Technical Publication Change Instructions

Updated replacement pages and/or drawings are attached to these Change Instructions. Please remove and discard the corresponding pages and/or drawings, and replace them with the attached pages and/or drawings. Failure to make these replacements may result in loss of product efficiency and possible failure.

Page numbers no longer have an alpha suffix, the revision level will now have a numerical suffix denoting its difference. Specific changes are identified by change bars in corresponding margins. A replacement page with no suffix has not been changed but is included only because it is part of the changed page.

Replacement pages will become standard pages without a suffix in the next printing of this manual and the Front Matter, Table of Contents, Preface and Index will be updated at that point. For record purposes, you are encouraged to retain these change instructions as a permanent part of the manual. Record new changes in your manual section entitled "Record of Changes".

Product:	50000B	Manual:	SERIES 5000B VXIBUS MICROWAVE SYNTHESIZERS OPERATION MANUAL	
Errata Issued:	July 24, 2001	Errata #:	31797-A1	
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Update your product technical manual. Replace the page(s) indicated below with their new revision level:

ECO(s):	Replace Page(s):	Remark(s):
7932	1-1 thru 1-2	N/A
	2-1 thru 2-4	
	2-7 thru 2-8	
	2-11 thru 2-12	
	2-15 thru 2-16	
	2-25 thru 2-26	
	3-5 thru 3-8	
	3-11 thru 3-22	
	Entire Chapter 4	Chapter 4 has to be entirely replaced, because of extended page and formatting of text, to fix this would affect readability.
	5-1 thru 5-2	N/A
	5-5 thru 5-12	
	A-1 thru A-2	Update to formatting in A.2.

Introduction

1.1 Description

The Giga-tronics VXIbus Microwave Synthesizers produces microwave signals with a high degree of frequency accuracy, frequency resolution and spectral purity. These signals may be controlled in amplitude over a wide range and are capable of being modulated in AM, FM and pulse modes. The product is designed to be installed in a VXI frame and to operate in the VXIbus environment.

The Giga-tronics VXIbus product line is designed to take advantage of the building block characteristics of the VXI system. The synthesizer is divided into discrete, C-size modules. There are two basic modules, which must always be present in any system. The first required module is the Control module (Model 52000B). This single width unit provides an interface to the VXI bus system and generates control signals for all other Giga-tronics modules. These control signals use the 12 local bus lines of the P2 connector. The Control module also provides a number of analog reference signals via front panel connectors.

The other module required for a minimum system is the double-width Synthesizer module (various model numbers in the 50000B/51000B series). Microwave frequencies are synthesized from the signals supplied by the Control module. The Synthesizer module contains all required circuitry and components to generate, modulate, and level the RF output.

Adaptor modules may also be included for optional features to the system.

Complete performance specifications for each module are presented in Section 1.2 in this chapter.

1.1.1 Items Furnished

In addition to options and/or accessories specifically ordered, items furnished with the instrument are as follows:

- 1 Operation Manual (P/N 31797)
- 1 Set of Reference Signal SMB-to-SMB cables (as required by modules)
- 1 or more RF semi-rigid cables (as required by optional modules)

1.1.2 Items Required

A VXI mainframe which meets the power and cooling requirements of the modules is required. Appropriate output cabling, which is made to fit the female SMA output connector, can be ordered in the form of Accessory A001 (Cable Kit).

1.1.3 Tools and Test Equipment

Special tools are not required in order to operate Series 50000B instruments. Signal sources for external modulation should match the parameters outlined in the specifications in this chapter. Test equipment required for calibration and testing is described in Chapter 4 of the manual.

1.1.4 Storage

Giga-tronics VXIbus modules should be stored in an environment free from excessive dust and dirt and where the temperature remains in the range of -40°C to +70°C.

1.1.5 Cooling

The specifications for individual modules define their cooling and airflow requirements. If the module is to be operated outside of a properly ventilated VXI frame, auxiliary air circulation is required, such as a small fan directed at the module.

1.1.6 Receiving Inspection

Use care in removing the instrument from the carton and check immediately for physical damage, such as bent or broken connectors on the front and rear panels, dents or scratches on the panels, broken extractor handles, etc. Check the shipping carton for evidence of physical damage and immediately report any damage to the shipping carrier.

Each Giga-tronics instrument must pass rigorous inspections and tests prior to shipment. Upon receipt, the instrument's performance should be promptly checked to ensure that its operation has not been impaired during shipment.

Each module is shipped in an operational condition and needs only to be plugged into a VXI frame to be used. A warm-up time of twenty minutes is recommended.

1.1.7 Safety Precautions

When installing modules into the mainframe, be sure that the connectors are properly aligned before pushing the modules into place. Use gentle but firm pressure to insert the modules and make sure they are fully seated for proper operation. In addition, make sure that the modules are installed in the correct positions relative to one another (see Positioning Requirements in Chapter 2).

1.1.8 Returning an Instrument

If it is necessary to return the instrument to the factory, protect the instrument during reshipment by using the best packaging materials available. If possible, use the original shipping container. If the original container is not available, use a strong carton (350 lbs./sq.in. bursting strength) or a wooden box. Wrap the instrument in heavy paper or plastic before placing it in the shipping container. Completely fill the areas on all sides of the instrument with packaging material. Take extra precaution to protect the front and rear panels. Seal the package with strong tape or metal bands. Mark the outside of the package: **"FRAGILE — DELICATE INSTRUMENT"**.

If corresponding with the factory or the local Giga-tronics sales office regarding reshipment, please provide the model and serial number. If the instrument is being returned for repair, be sure to enclose all relevant information regarding the problem that has been found.



NOTE: If you are returning an instrument to Giga-tronics for service, first contact Customer Service so that a return authorization number (RMA) can be assigned via e-mail at repairs@gigatronics.com or at **800.444.2878** (The 800 number is only valid within the US). You may also try our domestic line at **925.328.4650** or Fax at **925.328.4702**.

Operation

2.1 Installation

2.1.1 Control Module Address Settings

The Control module requires no pre-installation configuration and can be installed in any slot of the VXI frame (except Slot 0). Its VXI Logical Address is assigned by means of a DIP switch. The switch is accessible through an opening on the left side of the module.

The switch positions represent a binary number pattern from 0 to 255 (more than one bit switch can be set to 1). The bit switch nearest the bottom rail of the module is the least significant bit. The switch position marked **ON** (toward the back of the module) is tied to ground through a resistor and is interpreted as a binary 0. The **OFF** (forward) position is interpreted as a binary 1.

The factory setting for this address is all 1 bits (hex FF, decimal 255). In the VXI environment, this value specifies dynamic configuration, which means that at start-up the Slot 0 controller will first perform a roll call of fixed address devices and then assign free addresses to all dynamic configuration devices. This prevents address conflicts.

The Model 52000B Control module is the only Giga-tronics module recognized directly by the Slot 0 controller. All other Giga-tronics modules must be installed contiguously to the right of the Model 52000B Control module and are recognized via the VXI local bus (12 lines which are forwarded via the backplane and reserved for local purposes).

2.1.2 Address Settings for Other Modules

All of the other Giga-tronics modules require the selection of local addresses to differentiate them from one another. The address of each module is set by a row of switches (accessible from the outside of the module). However, in the case of a local address, these switches are not interpreted as a binary number. Only one of the eight switches should be in the ON (back) position at a time. The switches are labeled 0 - 7 and represent local addresses 0 - 7. Local addresses must be consecutive within a group of modules which work together.

The Synthesizer module should be placed to the immediate right of the Control module and should have the lowest address. The addresses of subsequent modules increase consecutively with the last module in the RF path having the highest address. The recommended arrangement is to set the Synthesizer module address to 0, the next module address to 1, and so on, so that the modules will be easy to identify for programming purposes.

Be sure that modules do not share the same address.

2.1.3 Inserting the Modules

After the module addresses are set, each module can be inserted into the VXI frame. Since the VXI local bus is not strapped across the entire width of the frame but only connects between the outer rows of the

P2 connector in adjacent slots, all Giga-tronics modules must be installed in one contiguous block. Also note that the next slot to the right of the last Giga-tronics module will have data appearing on its local bus lines. This should not cause a problem unless a module placed in that position uses those pins.

It will not cause a conflict if a second Giga-tronics Control module is placed to the right of a block of Giga-tronics modules. The Control module does not connect to the left direction local bus.

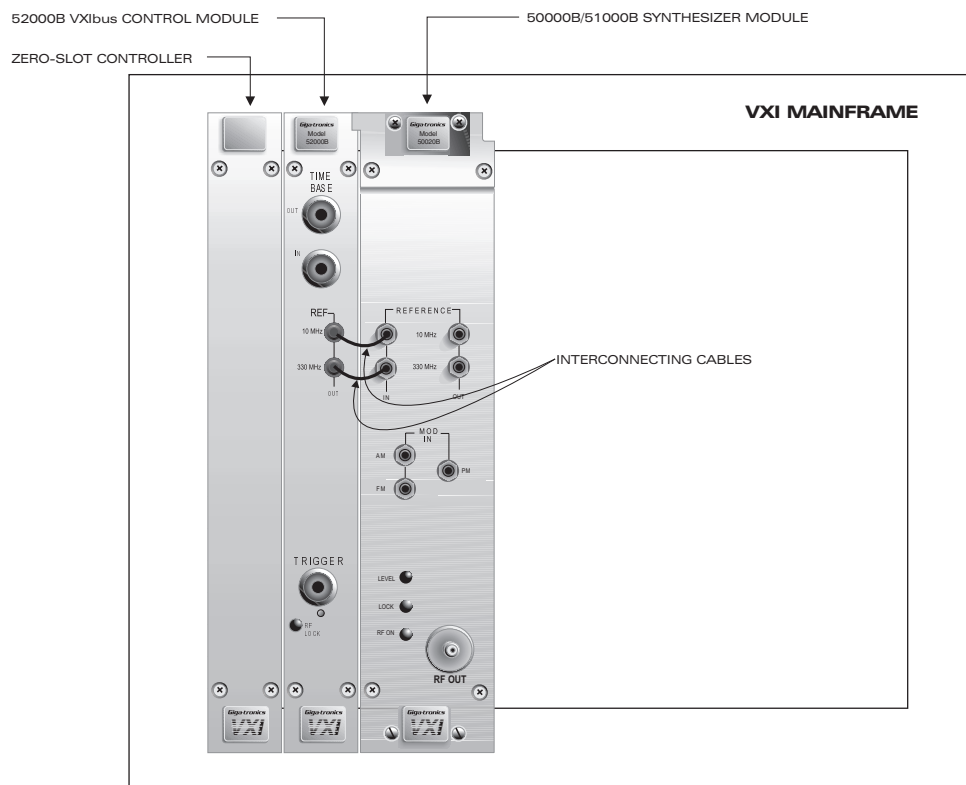


Figure 2-1: Module Mainframe Positions

2.1.4 Interconnection

Once the modules have been inserted in the VXI frame, use the supplied coaxial cables to connect the 10 MHz and 330 MHz signals (these are timebase-derived reference signals). These cables are required for proper interconnection of the Control module and any subsequent Synthesizer modules.

Begin by connecting the Control module 10 MHz output to the 10 MHz input on the first Synthesizer module. Likewise connect the 330 MHz line (see Figure 2-1). All cable assemblies are identical and can be used in any position. If there is more than one Synthesizer module in the system, connect the two signal outputs of the first module to the inputs of the next.

If it is required to place some other Giga-tronics module between two Synthesizer modules, longer cables can be fabricated using SMB female type connectors and a length of appropriate 50 ohm coaxial cable. Cable length should be no greater than is necessary to bridge the gap.

2.1.5 External Inputs

An external 10 MHz timebase can be connected to the Control module to allow the use of an external signal as a common system reference. The internal timebase is automatically disconnected when the external one is connected. The external timebase must have an amplitude of at least $1.5 V_{p-p}$ and must be accurate to within 1×10^{-6} .

The Synthesizer module has inputs which accept external modulating signals for AM, FM and PM. See the specifications in Chapter 1 for input parameters. The Synthesizer module includes a 10-pin Sweep Input connector, which accepts sweep control signals.

2.1.6 Connections to the VXI Mainframe

All modules connect to the backplane of the VXI mainframe through a pair of 96-pin connectors (P1 and P2). Pin assignments for these connectors are shown below.

Table 2-1: VXI Backplate Pinouts

Pin No.	P1 Connector			P2 Connector		
	Row A	Row B	Row C	Row A	Row B	Row C
1	D00	$\overline{\text{BBSY}}$	D08	ECLTRG0	+5V	CLK10+
2	D01	BCLR	D09	-2V	GND	CLK10-
3	D02	$\overline{\text{ACFAIL}}$	D10	ECLTRG1	RSV1	GND
4	D03	$\overline{\text{BG0IN}}$	D11	GND	A24	-5.2V
5	D04	$\overline{\text{BG0OUT}}$	D12	LBUSA00	A25	LBUSC00
6	D05	$\overline{\text{BG1IN}}$	D13	LBUSA01	A26	LBUSC01
7	D06	$\overline{\text{BG1OUT}}$	D14	-5.2V	A27	GND
8	D07	$\overline{\text{BG2IN}}$	D15	LBUSA02	A28	LBUSC02
9	GND	$\overline{\text{BG2OUT}}$	GND	LBUSA03	A29	LBUSC03
10	SYSCLK	$\overline{\text{BG3IN}}$	$\overline{\text{SYSFAIL}}$	GND	A30	GND
11	GND	$\overline{\text{BG3OUT}}$	$\overline{\text{BERR}}$	LBUSA04	A31	LBUSC04
12	$\overline{\text{DS1}}$	$\overline{\text{BR0}}$	$\overline{\text{SYSRESET}}$	LBUSA05	GND	LBUSC05
13	$\overline{\text{DS0}}$	$\overline{\text{BR1}}$	$\overline{\text{LWORD}}$	-5.2V	+5V	-2V
14	$\overline{\text{WRITE}}$	$\overline{\text{BR2}}$	AM5	LBUSA06	D16	LBUSC06
15	GND	$\overline{\text{BR3}}$	A23	LBUSA07	D17	LBUSC07
16	$\overline{\text{DTACK}}$	AM0	A22	GND	D18	GND
17	GND	AM1	A21	LBUSA08	D19	LBUSC08
18	$\overline{\text{AS}}$	AM2	A20	LBUSA09	D20	LBUSC09
19	GND	AM3	A19	-5.2V	D21	-5.2V
20	$\overline{\text{IACK}}$	GND	A18	LBUSA10	D22	LBUSC10
21	$\overline{\text{IACKIN}}$	SERCLK	A17	LBUSA11	D23	LBUSC11
22	$\overline{\text{IACKOUT}}$	$\overline{\text{SERDAT}}$	A16	GND	GND	GND
23	AM4	GND	A15	$\overline{\text{TTLTRIG0}}$	D24	$\overline{\text{TTLTRIG1}}$
24	A07	$\overline{\text{IRQ7}}$	A14	$\overline{\text{TTLTRIG2}}$	D25	$\overline{\text{TTLTRIG3}}$
25	A06	$\overline{\text{IRQ6}}$	A13	+5V	D26	GND
26	A05	$\overline{\text{IRQ5}}$	A12	$\overline{\text{TTLTRIG4}}$	D27	$\overline{\text{TTLTRIG5}}$
27	A04	$\overline{\text{IRQ4}}$	A11	$\overline{\text{TTLTRIG6}}$	D28	$\overline{\text{TTLTRIG7}}$
28	A03	$\overline{\text{IRQ3}}$	A10	GND	D29	GND
29	A02	$\overline{\text{IRQ2}}$	A09	RSV2	D30	RSV3
30	A01	$\overline{\text{IRQ1}}$	A08	MODID	D31	GND
31	-12V	+5V STDBY	+12V	GND	GND	+24V
32	+5V	+5V	+5V	SUMBUS	+5V	-24V

2.3.3 Command Set

The command set for the HP-style syntax is listed in the following tables. The commands are discussed in alphabetical order with some related commands grouped together.

Commands *CLS through *WAI (IEEE 488.2 Common Commands)

See the SCPI section for more information about these commands.

Table 2-2: Commands *CLS - *WAI

Command	Description
*CLS	Clear Status
*ESE	Event Status Enable
*ESE?	Event Status Enable Query
*ESR?	Event Status Register Query
*IDN?	Identify
*OPC	Operation Complete
*OPC?	Operation Complete Query
*RST	Reset
*SRE	Status Register Enable
*SRE?	Status Register Enable Query
*STB?	Status Byte Query
*TST?	Self-Test Query (see the self-test commands, TA etc.).
*WAI	Wait-to-Continue

Commands AM0 through FM1 (Miscellaneous)

Table 2-3: Commands AM0 - FM1

Command	Description
AM0	Deactivate external AM.
AM1	Activate external AM.
AMF0	Deactivate external fast AM.
AMF1	Activate external fast AM.
CIIL	Switch to CIIL language.
CW d t	Select the CW (fixed frequency) mode.
DN	Down step of frequency or power level, depending on whether the last command was CW (Frequency) or PL (Power).
[Down step of frequency or power level, depending on whether the last command was CW (Frequency) or PL (Power).
FM0	Deactivate external FM.
FM1	Activate external FM.

Commands GA through GR (FSD Commands)

Frequency Sweep Digital (FSD) commands permit the setup then activation of digital frequency sweep. Depending on the sweep triggering method chosen, the sweep can begin immediately upon receipt of the activation command or after the activation command followed by a definable hardware trigger signal. The sweep can be single or continuously repetitive. The next frequency is obtained either by adding the step size increment to the last frequency or by retrieving the next frequency value from a list stored in memory.

Table 2-4: Commands GA - GR

Command	Description
GA d t	Set the sweep start frequency to d GHz. Default: minimum frequency.
GB d t	Set the sweep stop frequency to d GHz. Default: maximum frequency.
GC d t	Set the frequency step size to d GHz. Default: 1 GHz.
GD d t	Set the dwell time to d seconds. Default: 1 s.
GEI	Start the sweep immediately upon receipt of a GG command (this is the default sweep triggering mode).
GEWF	Start the sweep (following receipt of a GG command) when the hardware trigger input goes to the FALSE level (0 V).
GEWT	Start the sweep (following receipt of a GG command) when the hardware trigger input goes to the TRUE level (+5 V).
GFC	Select the continuous sweep mode (the sweep repeats automatically).
GFR	Select the retriggerable single sweep mode (the sweeper will respond to another trigger occurring after completion of the sweep).
GFS	Select the single sweep mode (the sweeper will NOT respond to another trigger occurring after completion of the sweep).
GG	Start the sweep. This command should be entered only after all the setup commands have been entered with the desired values. If the GEI command was sent previously, the GG command will cause the sweep to begin immediately. If the GEWF or GEWT command was sent, the GG command will cause the sweeper to wait for the appropriate hardware trigger input.
GH	Halt the sweep, leaving the frequency at the last stepped value (NOTE: a CW command will also halt the sweep).
GIM	Memory increment mode: increment the frequency by going to the next nonzero frequency stored in an array of up to ten memory locations (see the GJ command). The start frequency, stop frequency, and step size have no effect in this mode, but the dwell time does apply.
GIN	Normal increment mode: increment the frequency by adding the defined step size to the last frequency (see the GC command). The start frequency, stop frequency, step size, and dwell time all apply in this mode.
GJ n d t	Save a sweep frequency (d) at memory location n (the range of values for n is 0 - 9). If the value saved at any memory location is zero, that memory location will have no effect on the sweep.
GK	Clear all saved sweep frequencies from memory (see the GJ command).
GR	Resume a sweep that was halted by a GH command.

Commands TA through TSD (Self Test Commands)

These commands all relate to the instrument's self-test routine.

Table 2-9: Commands TA - TSD

Command	Description
TA	Abort the test.
TFB d t	Set the beginning frequency for the test to d. Default: minimum frequency.
TFE d t	Set the ending frequency for the test to d. Default: maximum frequency.
TFS d t	Set the frequency step size for the test to d. Default: 1 GHz.
TFQ?	Test frequency quit query (at what frequency did the test stop?). The test quits when a failure is detected. Default: 0 (test not yet run).
TPC d t	Set the coarse power level for the test to d dBm. This specifies the setting of the step attenuator (from 0 dBm to maximum attenuation in 10 dB steps) during the test. Default: 0 dBm.
TPF d t	Set the fine power level for the test to d dBm. This specifies the setting of the leveling loop in 0.1 dB increments from -20 dBm - +20 dBm. Default: maximum leveled power.
TSB?	TST Status Binary Query.
TSD?	TST Status Decimal Query.
Related Commands	
*TST?	Self-Test Query
RT	Run self-test is a lock-and-level test of the synthesizer operation across a defined frequency range.

The *TST? command (an IEEE 488.2 Common Command) will preserve (it will save and later restore) these states:

- RFx** RF On/Off state
- CWx** CW Frequency value
- PCx** Power Level (Coarse) value
- PFx** Power Level (Fine) value

The test will then switch in the maximum step attenuation before doing its own testing to not damage any user circuitry at the RF output connector. The Power Level (fine) value during the test will be the maximum output value for the unit (usually 10 dBm), but the Power Level (coarse) is usually -90 dB. The connector output power is the sum of the two, which is small enough that it presents no risk of damage.

The *TST? command always returns a decimal value result. If the returned value is 0, the test ran without errors. If not, the value is the sum of a series of weights as will be explained later.

The RT command resembles the *TST? command but differs in two respects. The RT command does not reply (separate commands are provided to request results afterward.) The RT command stops at its last frequency, and does not remember the original frequency from before the test was run.

You must separately request the results of the RT command. You might also want to request again the reply of the *TST? command in a different format. Two queries are provided for different style results.

The TSB? (Test Status Binary) query requests the result as a series of ASCII characters; each is either a 1 or a 0. The characters are in order and each one has a specific meaning. For any condition, 1 means the particular condition is satisfactory and 0 means it is not satisfactory. A test that runs without errors will return a TSB? of 11111111.

The TSD? (Test Status Decimal) query requests the same result expressed as a decimal number. If the returned value is 0, the test ran without errors. If not, the value is the sum of a series of weights which depend upon what type of hardware makes up the device. The inclusion of a particular condition's weight in the sum means the condition is not satisfactory.

The bit/weight meanings in the test status reply are the same whether the result is queried by a TSB? or a TSD? command, as illustrated in Table 2-10.

Table 2-10: Bit/Weight Meanings

Bit	Weight	Meaning
7	128	Leveled
6	64	Downconverter Loop Locked
5	32	110 MHz Loop Locked
4	16	Output Loop Locked
3	8	300 MHz Loop Locked
2	4	80 MHz Loop Locked
1	2	(not used)
0	1	(not used)

If you inadvertently enter a very small step size and then start the test running, the abort command (TA) provides a way of stopping it before completion. The test is simply stopped. If you had issued the *TST? command, no reply will occur after abort. You must manage the clearing of your expected reply.

With the *TST? command, you simply wait for the reply. With the RT command, you must be sure the test is done before requesting its status via TSB? or TSD?. The easiest way to do this is by using the *WAI command to wait until the test is done. You might prefer *OPC or *OPC?. Current firmware requires that the coordination command be on its own command line; likewise for the following TSB? or TSD? command.

Commands UL0 through] (Miscellaneous)

Table 2-11: Commands UL0 through]

Command	Description
UL0	Unleveled mode off
UL1	Unleveled mode on
UP	Up step for CW (Frequency) or PL (Power)
]	Up step for CW (Frequency) or PL (Power)

2.5 SCPI Syntax

The SCPI syntax is now implemented in the 50000B Series. It includes the IEEE 488.2 Common commands, status reporting, error reporting, and table-specified defaults at power-up or *RST.

2.5.1 SCPI Command Format

Details of typography (such as indentation, case, and punctuation) are very significant in SCPI and must be attended to with great care. The typographic conventions employed in the SCPI command tables which follow are summarized here.

Colons indicate changes of level in the SCPI tree structure. If a command is represented in the format ALPHA:BETA:GAMMA, then BETA is one level down from ALPHA, and GAMMA is two levels down from ALPHA. If ALPHA is printed at the left margin, ALPHA is at the root level. In the command tables, indentation indicates relative levels.

Commands can be entered in upper or lowercase. However, only required letters are in upper case in the command table. If you enter more than the required letters, you must enter the entire command (if the command is INITiate, you may use either INIT or INITIATE, but INITI is invalid).

If a command is shown in square brackets, it is an implied command and can be omitted (the brackets are not part of the command and should be omitted even if the command itself is entered). An implied command is the default command among the commands available at its level. For example, in the case of the command INITiate:[IMMEDIATE], the immediate mode is the default mode, so entering INIT has the same effect as entering INIT:IMM.

Because you can query any value that you can set, most commands also exist in a query form (signified by adding a question mark to the end of the keyword). The command tables do not contain separate listings for queries except in the case of commands that exist only in the query form. If there is a command ALPHA, you can assume that there is also an ALPHA? query unless the table entry includes the statement NO QUERY. Some commands are events that cause something to happen at a particular time but do not create a setting or value to be checked afterwards. Consequently, they have no query form.

Some commands require a parameter. The parameter types are:

BOOL:A Boolean (true or false) condition. Enter

ON or 1 for TRUE;
OFF or 0 for FALSE.

VAL:A numeric value or a qualitative term which represents a numeric value. Enter:

sign (optional),
digits,
decimal point (optional),
E xx (optional),
units suffix (optional).
Or enter MIN, or MAX.
Or enter UP, or DOWN (these only change the synthesizer's output frequency or output power level).

NUM:A number (typically represents register bit settings in the form of a decimal integer).

There are also discrete parameters. These are options to be chosen from a limited selection. For example, the TRIGger:SLOPe command has three possible discrete parameters to choose from (POSitive, NEGative, and NONe). The beginning of a parameter must be preceded by a space. The default units suffixes are DBM for power and HZ for frequency (the other suffixes for frequency are GHZ, MHZ, and KHZ).

2.5.2 SCPI Commands

Tables 2-13 through Table 2-17 list the SCPI commands with notes on parameter types, initial values, and whether or not a query form of the command exists. The effect of the command is explained below each command listing. Many of these commands refer to the Status System, which is discussed in detail in Section 2.6. Commands beginning with an asterisk are IEEE 488.2 Common Commands.

Table 2-13: SCPI Commands CLS - TST

Keyword	Parameter Type	Initial Value	Query Form?
*CLS	none	none	no
(Clear Status Command) This command clears the event registers in all status groups. It also clears the Event Status Register and the Error/Event Queue.			
*ESE	NUM	0	yes
(Standard Event Status Enable Command) This command make it possible for specified changes in the Standard Event Status Register to generate service requests. The query form (*ESE?) determines which changes in the Standard Event Status Register have been enabled to generate service requests. The parameter is a decimal number which represents the register's bit settings.			
*ESR?	none	0	query only
(Standard Event Status Register Query) This command causes the event register of the Standard Event Status Register group to be read and transmitted over the bus		It also causes the register to be cleared.	
*IDN?	none	none	query only
(Identification Query) The response takes the form of four ASCII fields separated by commas. The fields are: (1) Manufacturer, (2) Model, (3) Serial Number, and (4) Firmware Level or Equivalent. Fields 1 and 2 are required; fields 3 and 4 are filled by zeros if the data is not available.			
*OPC	none	none	yes
(Operation Complete Command) This command causes the Operation Complete bit (that is, Bit 0 of the Standard Event Status Register) to be set to 1 when all pending selected device operations have been finished. The query form (*OPC?) places an ASCII character 1 into the device's output queue when all pending selected device operations have been finished. Unlike the *OPC command, the *OPC? query does not affect the OPC Event bit in the Standard Event Status Register (ESR).			
*RST	none	none	no
(Reset Command) This command sets the device-specific functions to a known state (the power-on state) that is independent of the past-use history of the device. The command does not reset any part of the status reporting system.			
*SRE	NUM	0	yes
(Service Request Enable Command) This command makes it possible for service requests to be generated by specified bits of the Status Byte Register. The query form (*SRE?) determines which bits of the Status Byte Register have been enabled to generate service requests.			
*STB?	none	none	query only
(Status Byte Query) This command causes the event register of the Status Byte Register group to be read and transmitted over the bus. It also causes the register to be cleared.			
*TST?	none	none	query only
(Self-Test Query) This command causes the synthesizer to perform a self-test routine. See the notes below concerning Self-Test.			

2.5.6 Sample SCPI Commands

Table 2-19 shows some examples of brief SCPI commands:

Table 2-19: Sample SCPI Commands

Command	Meaning
*IDN?	Query instrument identification (response format: maker,model,serial#,firmware version; (sample response: Giga-tronics,50000,048256,75).
*RST	Reset system.
OUTP OFF	Turn off RF output.
AM:STAT OFF	Turn off external amplitude modulation.
AM:STAT?	Query external amplitude modulation (sample response: 0).
POW -9.2	Set output power to -9.2 dBm.
POW?	Query output power (sample response: -9.2).
FM:STAT OFF	Turn off external frequency modulation.
FM:STAT?	Query external frequency modulation (sample response: 0).
FREQ 6.1GHZ	Set output frequency to 6.1 GHz
FREQ?	Query output frequency (sample response: 6100000000).
PULM:STAT OFF	Turn off external pulse modulation.
PULM:STAT?	Query external pulse modulation (sample response: 0).

2.6 SCPI Status System

2.6.1 Introduction

The SCPI standard includes a system for monitoring the status of the instrument. Much of this status system is imported from the IEEE 488.2 standard. Status monitoring is accomplished by means of several registers which can be read from (or in some cases written to). Registers of various kinds are combined into status groups and the status groups are nested: the output bits of a status group are summarized by a logical-OR gate. The summary output becomes one of several inputs to another status group. The various groups and registers are described in detail below.

SCPI terminology is not consistent. The distinction between a register and a group of registers is often ignored. Some status groups are called status registers. This manual does not attempt to correct SCPI's choice of words, but confusions of this kind will be pointed out where they occur.


2.6.2 Registers, Bit Numbers, and Decimal Weights

When a register is read, its bit settings are converted into a single decimal number for transmission over the interface. The decimal weights for the various bits are shown in Table 2-20 below:

Table 2-20: Bit Numbers and Decimal Weights

Bit:	7	6	5	4	3	2	1	0
Weight:	128	64	32	16	8	4	2	1

If Bit 0 (the least significant bit) is ON, its weight is 1. If Bit 7 (the most significant bit) is ON, its weight is 128. If 0 and 7 were the only bits ON, the register would have a decimal value of 129 (the sum of the weights). If all bits were ON, the register would have a decimal value of 255.

 **NOTE:** Although SCPI defines some registers as having 16 bits, Giga-tronics makes use of only the lowest 8 bits of any register. Therefore, every register can be treated as if it contained only 8 bits.

To determine which bits are on from the decimal value, find the largest weight that does not exceed the decimal value. Subtract that weight from the value and mark that bit ON. Continue subtracting weights, and marking the associated bits ON until the decimal value is reduced to zero.

EXAMPLE:

- The decimal value is 235.
- Subtract 128 and mark Bit 7 ON. The decimal value is now 107.
- Subtract 64 and mark Bit 6 ON. The decimal value is now 43.
- Subtract 32 and mark Bit 5 ON. The decimal value is now 11.
- Subtract 8 and mark Bit 3 ON. The decimal value is now 3.
- Subtract 2 and mark Bit 1 ON. The decimal value is now 1.
- Subtract 1 and mark Bit 0 ON. The decimal value is now 0.
- Conclusion: Bits 7, 6, 5, 3, 1, and 0 are ON. Bits 4 and 2 are OFF.

This procedure is done in reverse in order to convert bit settings to a decimal value. Add together the decimal weights (as shown in Table 2-20) for each bit which is ON to find the equivalent decimal value.

3.2 Amplitude Control

Amplitude control of the Synthesizer output is adjusted by a combination of fixed-step attenuation and closed-loop leveling (in the ALC). The fixed-step attenuation is done by a step attenuator providing up to 90 dB of attenuation in 10 dB increments. Closed-loop leveling is accomplished through Automatic Leveling Control (ALC), which provides fine adjustment in 1 dB increments.

3.2.1 The ALC Circuit

The ALC is basically a loop amplifier with multiple inputs. One of the inputs takes feedback from the level detector (a circuit that returns a negative voltage proportional to the square of detected power). The RF measured by the detector is coupled from the output path by a circuit in the RF module. The detector signal is amplified and applied to the summing junction of the leveling loop amplifier; it is a variable input in that it changes in response to the loop amplifier output.

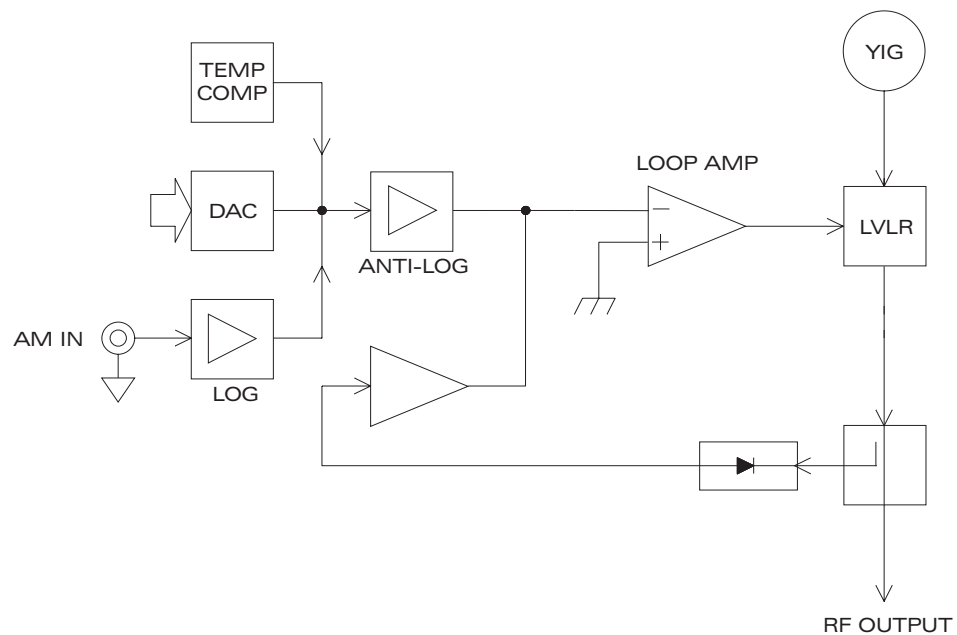


Figure 3-3: Amplitude Control

Another input into the ALC is the reference input. The reference input is a composite of three signals: a correction voltage from the temperature compensation circuit (PC board A3), a fixed leveling input (which the Control module programs by means of a digital to analog converter) and the AM signal from the front panel input. If present, the AM signal is processed by a logarithmic amplifier in order to give it the same logarithmic characteristic as the other two inputs. Then, all three signals can be combined by a summing amplifier; the combined signal is processed by an anti-logarithmic amplifier on its way to the loop amplifier.

The ALC output is sent to an amplifier which drives the PIN diode leveler so as to balance the reference input against an equal and opposite variable feedback input. In other words, the leveler adjusts RF power until the detector feedback input just cancels the other input to the loop amplifier.

In setting the leveling reference, through the programming of a digital to analog converter, the Control module includes compensation factors from a level-characterization table (stored in a PROM in the Synthesizer module). This data is individual to each synthesizer system and is compiled during production testing.

3.2.2 Amplitude Modulation

The AM input to the level control circuit supplies the leveling loop amplifier with a variable, rather than a fixed leveling reference. The variable reference is processed by a log amplifier in order to match the logarithmic characteristics of the computer leveling reference and the temperature compensation input. The level control circuit furnishes a modulated control voltage to the leveler in the RF module to match the modulation of the reference input. The result is an amplitude modulated RF output with a modulation depth of at least 20 dB.

3.3 Pulse Modulation

Pulse modulation is performed by means of path-switching circuits in the RF module. Depending on output bandwidth, there will be up to five filter paths through the module (only one is active at a given time). PIN diode circuits switch these lines on and off; pulse modulation is accomplished by shutting off the active path intermittently. (A positive voltage at the filter line control pin on the outside of the module shuts the path off.) By this method, an on/off ratio of greater than 80 dB can be achieved.

3.4 Frequency Modulation

Frequency modulation of the RF output is achieved by modifying the fine tuning of the YIG oscillator. The current supply to the YIG's fine tuning coil is controlled by the FM driver (Part of A2), which in turn, is controlled by the output phase lock loop circuit (Part of A2). Normally, the PLL driver output, suitably filtered and amplified, is derived from the outputs of the phase comparator. However, during operation in the FM mode, this phase comparator signal is summed with a modulation signal. The outcome is a modulated drive resulting in a frequency modulated output from the YIG oscillator.

3.5 Frequency Synthesis

The output frequency is produced by a YIG oscillator. Coarse tuning of the YIG is done through the YIG driver (A3). The A3 circuit board supplies a programmable current source which the Control module adjusts by means of a digital to analog converter and amplifier. This current source, connected to the YIG tuning coil, can bring the YIG frequency within 50 MHz of the desired value. Fine tuning of the YIG is accomplished by the output phase lock loop, which supplies a controlled tuning current to the YIG's FM coil. The overall synthesis process can involve up to six phase lock loops, depending on output frequency resolution.

3.5.1 Phase Lock Loop

The purpose of a phase lock loop (PLL) is to control a variable frequency oscillator so that its output frequency has the same accuracy and stability as that of a fixed reference oscillator.

The PLL works by comparing two frequency inputs, one fixed and one variable. After comparison, it supplies a correction signal to the variable oscillator achieving and maintaining a constant phase relationship between the two inputs (see Figure 3-4).

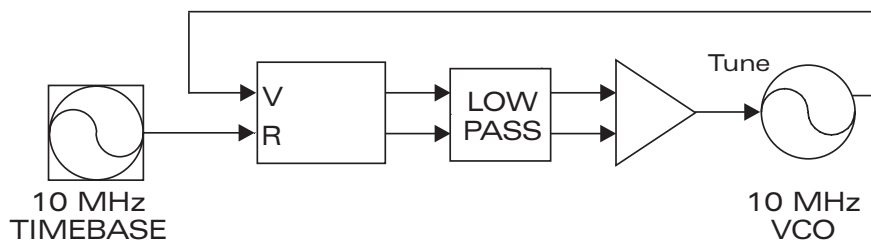


Figure 3-4: Elementary Phase Lock Loop

The stability and accuracy of a reference frequency (for example, the signal produced by a 10 MHz crystal oscillator) can be transferred to a voltage controlled oscillator (VCO) by means of a phase lock loop. The 10 MHz signal is applied to the reference input of the PLL, and the VCO output frequency is fed back to the variable input of the PLL. A phase detector in the PLL circuit compares the two inputs and determines whether the variable input is leading, or lagging, the reference. The phase detector has two outputs. Pulses appear at one output, depending on whether the variable input is leading or lagging. (The width of the pulses is proportional to the degree of phase difference.) The width of the pulses are averaged by a low pass filter and DC amplifier; the result is a correction signal causing the VCO frequency to increase, or decrease, in order to reduce the phase difference between the two input frequencies. When the phase error is eliminated: the frequencies are equal, the loop is said to be locked, and the VCO frequency acquires the accuracy and stability of the reference input.

Although the variable input to the phase detector should equal the frequency of the reference input, it need not equal the frequency of the VCO. If a frequency divider is introduced between the VCO and the variable input, the VCO can be run at a frequency that is a multiple of the reference frequency. For example, if the VCO output is divided by ten before being applied to the phase detector input, the VCO can run at 100 MHz and still be phase locked to a 10 MHz reference. A frequency divider intervening between the VCO and the phase detector variable input is called a prescaler. If the prescaler is programmable (i.e., it can be set to a given divisor), a variety of frequencies can be phase locked to a single reference frequency (see Figure 3-5).

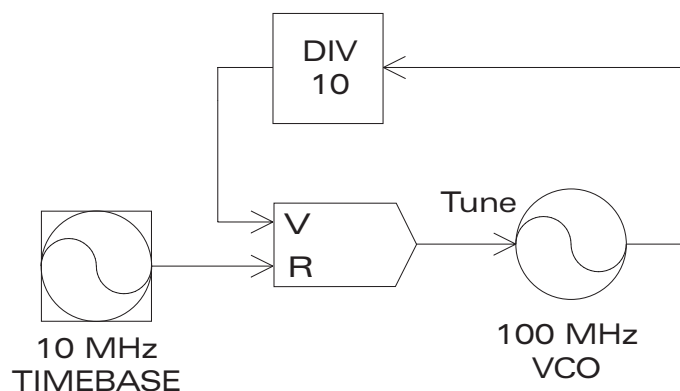


Figure 3-5: Phase Lock Loop, with Prescaler

Since the output frequency must be some multiple of the reference frequency input to the phase detector; the reference frequency limits the resolution of the system. For example: using a 10 MHz timebase, frequencies of 70 MHz, or 80 MHz, can be generated. However, frequencies of 73 MHz cannot be generated, because digital frequency dividers can perform integer divisions only (i.e., the prescaler cannot be programmed to divide by 7.3). Nevertheless, if the reference frequency applied to the phase detector is itself programmable, this difficulty can be overcome. The solution is to use a 1 MHz reference frequency and divide the output by 73, or use a 7.3 MHz reference and divide the output by 10.

3.5.2 Microwave Frequency Synthesis

Digital synthesis of microwave frequencies is impeded by two inherent difficulties. First, these frequencies are well above the operating range of digital logic circuits. Secondly, the bandwidths required tend to be large (several thousand Megahertz). A requirement for fine frequency resolution over so wide of a range further complicates the synthesis process.

Because the Synthesizer output frequency is too high for digital circuits to work with, the Synthesizer uses RF mixers to downconvert microwave signals to a lower and more workable range. Generally, a mixer provides an intermediate frequency equal to the difference between two high-frequency inputs. For example, a step-recovery diode multiplier and an RF mixer (used in a combination known as a sampling mixer) can derive a low frequency I.F. equal to the difference between the output microwave signal and some harmonic of a stable reference frequency. The various reference signals used to synthesize the output are generated at, or mixed down to, frequencies low enough to drive digital circuits.

The problem of bandwidth, insofar as it limits frequency resolution, is overcome through the use of several compounded PLL circuits, which produce reference frequencies programmable in 1 kHz increments over a wide range.

3.5.3 The Synthesis Network

All output frequencies are synthesized by the output PLL, and are ultimately phase locked to the 10 MHz master reference. The Synthesizer can be analyzed as two parallel branches connecting the master reference to the output PLL reference and variable inputs. The variable branch includes feedback from the output YIG oscillator. *Unless otherwise noted all circuits are located in the Synthesizer module.*

80 MHz PLL (A1)

The 80 MHz PLL is used to generate a fixed 80 MHz output which is phase locked to the timebase. The 80 MHz VCO is tuned by the output of a phase comparator. The VCO output is fed back to the phase comparator's variable input by way of a divide-by-eight circuit (so that the variable input is 10 MHz when the loop is locked). The phase comparator's reference input is the 10 MHz timebase.

The fixed 80 MHz output of the VCO is used as a reference input by the Direct Digital Synthesizer (DDS) chip. The DDS is used in conjunction with a Digital-to-Analog Converter to generate a programmable output frequency in the range of 3 to 20 MHz. The output frequency is programmed digitally by the CPU; the DDS generates a sequence of digital values which is converted into a waveform by the DAC. (The DAC, too, is clocked by the 80 MHz reference input.) The DAC's output is amplified and furnished (through a low-pass filter which removes noise generated by the digital circuits) to the reference input of the Output PLL.

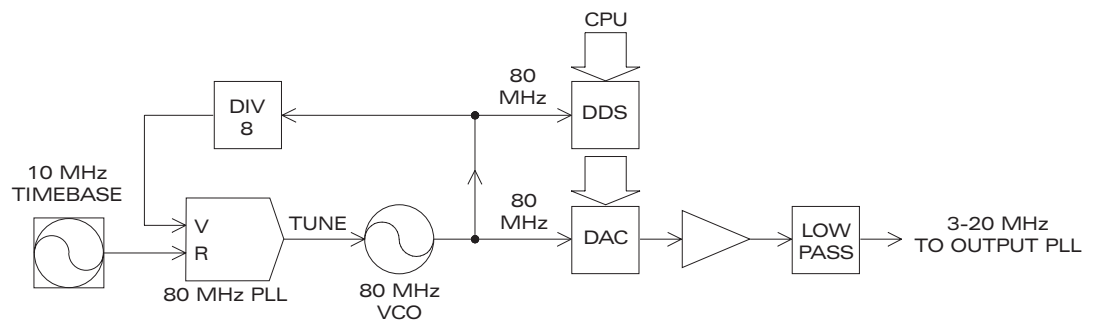


Figure 3-8: 80 MHz PLL and DDS

3.5.5 The Variable Branch

This branch consists of circuits in the following sequence:

- 10 MHz master reference (Control module)
- 110 MHz PLL (Control module)
- 110 MHz oscillator/multiplier (Control module)
- 300 MHz PLL (A2)
- 300 MHz VCO/driver (A104)
- Sampling mixer/IF amplifier (A104)
- Divide-by-N (A2)
- Output PLL, variable input (A2)

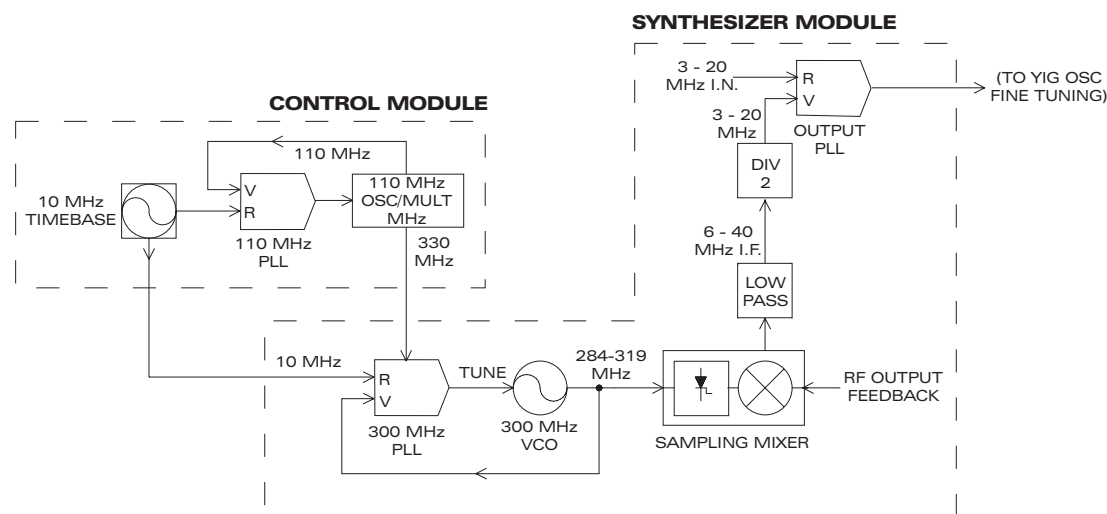


Figure 3-9: The Variable Branch

The 10 MHz master reference and the 110 MHz PLL are the same circuits used in the reference branch.

The 110 MHz oscillator/multiplier supplies a 330 MHz reference input to the 300 MHz PLL.

The 300 MHz PLL and the 300 MHz VCO/driver function together as a programmable source, generating frequencies in 1 MHz steps between 284 and 319 MHz (the 300 MHz PLL/VCO combination is described in more detail on the following page). This 284 to 319 MHz output is amplified and furnished to the multiplier input of the sampling mixer.

The sampling mixer has a step recovery diode multiplier on one of its inputs (the input driven by the 300 MHz VCO): the multiplier produces a series of frequency components that are harmonics of the input. The other input to the mixer is an RF feedback signal, coupled from the output of the YIG oscillator. The mixer combines the YIG frequency with the harmonics of the VCO frequency, yielding a great variety of intermediate frequency (IF) components. The IF output is amplified and filtered in order to pass only IFs within an 80 MHz range. In this way the output is limited to a single IF component

derived from the difference between the YIG frequency and one of the VCO's harmonics. The IF (a signal programmable over a range of 6 to 40 MHz) is applied to the divide-by-2 circuit.

The divide-by-2 circuit produces an output frequency in the range of 3 to 20 MHz. The output is applied to the variable input of the output phase lock loop. The amplified and filtered phase detector output of the PLL is further amplified by the FM driver circuit before being applied to the YIG's FM coil. The YIG is tuned in order to adjust the sampling mixer's IF and thus equalize the reference and variable inputs to the PLL.

The various programmable frequencies are set by the Synthesizer Control module, in accordance with a complex algorithm, to produce the requested output frequency.

300 MHz PLL/VCO

The 300 MHz PLL/VCO portion of the variable branch consists of an oscillator, a mixer, two dividers, and a phase comparator (see Figure 3-10). The VCO's frequency output is fed back to the mixer, and mixed with the 330 MHz reference input. The resulting IF equals the difference between the VCO's frequency and 330 MHz; since the VCO has a range of 284 to 319 MHz, the IF has a range of 11 to 46 MHz.

The IF is furnished to a programmable divider. The divider is programmed with whatever divisor is needed to reduce the desired IF to 1 MHz (in other words, if the desired IF is 25 MHz, the divisor is set to 25). The 1 MHz output of the divider is applied to the variable input of the phase comparator (of course, the output of the divider will equal 1 MHz only when the loop is locked).

The reference input to the phase comparator is a fixed 1 MHz signal, produced by dividing the 10 MHz timebase signal by ten. The comparator's output drives the VCO in whatever direction will reduce the difference between the fixed 1 MHz input and the output of the divider.

The frequency of the VCO is determined by the setting of the programmable divider. If the divisor is set to 11, the VCO will be driven by the phase comparator to 319 MHz, resulting in an 11 MHz IF and a 1 MHz input to the phase comparator. If the divisor is set to 46, the VCO will be driven to 284 MHz, resulting in a 46 MHz IF and a 1 MHz input to the phase comparator.

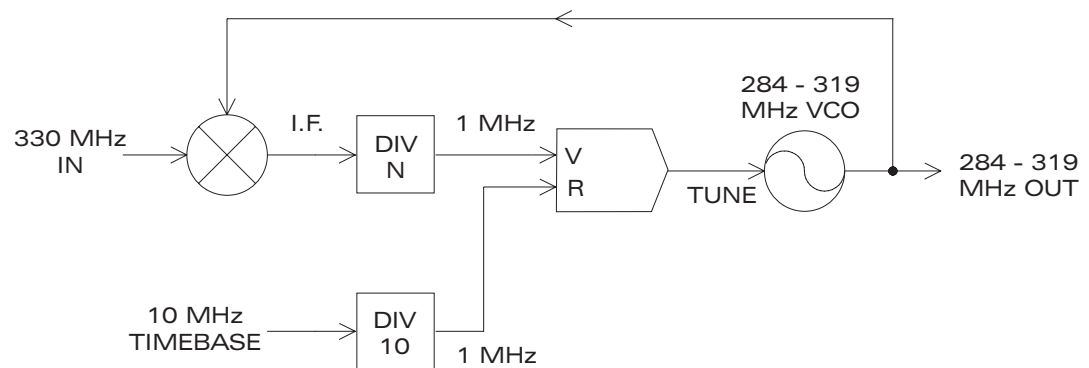


Figure 3-10: 300 MHz PLL/VCO

3.5.6 The Downconverter

The downconverter extends the frequency range of the Synthesizer module downwards, to 10 MHz. The downconverter is needed because its .01 to 2 GHz range is too low to be generated by a YIG oscillator (see Figure 3-11). The downconverter circuit mixes the YIG frequency with the fixed output of a local oscillator, yielding an intermediate frequency output in the range of .01 to 2 GHz.

The downconverter circuit is part of the main RF module. During operation below 2 GHz, a coupler in the output path diverts some RF from the module to the downconverter; the low frequency signal synthesized by the downconverter is returned to a switch and furnished to the step attenuator.

During operation in the downconverter range, the YIG oscillator is tuned to a frequency in the approximate range of 5.9 to 7.9 GHz. The downconverter switch furnishes this frequency to the downconverter mixer. The other input to the mixer is a fixed 7.920 GHz input from a Dielectric Resonant Oscillator (DRO). The DRO output is phase-locked to the 330 MHz reference signal applied to it; the 330 MHz reference is in turn phase-locked to the instrument's 10 MHz master reference.

The IF output from the mixer is equal to the difference between the YIG frequency and the 7.920 GHz fixed output of the DRO. For example, the IF is 1.000 GHz when the YIG frequency is 6.920 GHz; the IF is .01 GHz when the YIG frequency is 7.910 GHz). The computer tunes and locks the YIG oscillator to the frequency that will yield the desired IF output from the downconverter mixer. The IF is amplified and returned to the downconverter switch.

Instrument functions, including level control and modulation, operate normally in the downconverter range (the leveling and modulation of the RF input to the downconverter mixer from the RF module is reflected in the mixer's IF output). The frequency synthesis process for the YIG frequency is also normal, except that it yields a frequency equal to 7.920 GHz minus the required output frequency.

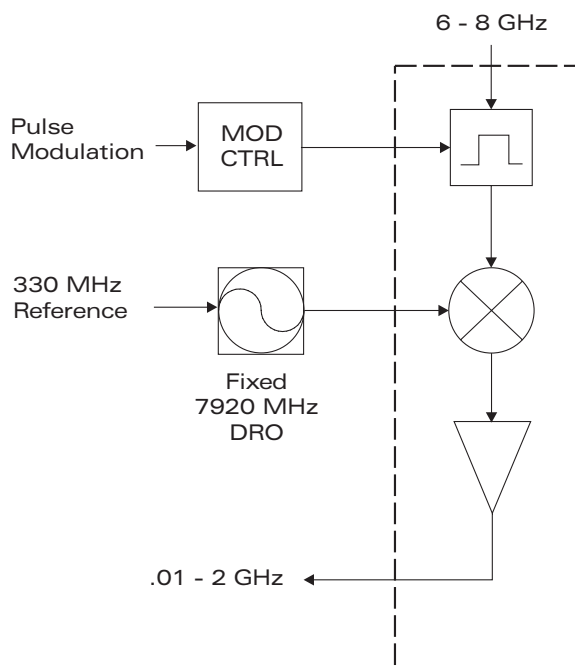


Figure 3-11: Downconverter Circuit

3.6 Circuit Descriptions (Controller)

3.6.1 VXI/Interface Control (A1)

This PC assembly is the only assembly in the Series 50000B that actually talks on the VXI bus. The A1 board holds the DT9150 Interface Technology daughter card, which handles all VXI Bus interface and communication. L1 thru L4 and associated capacitors provide filtering of the +5V supply to this assembly.

In addition to providing VXI bus interface functions, the microprocessor on this board runs the software contained in the U6 and U7 PROMS to control the 50000B modules. This software uses the U13 Peripheral Interface Timer IC 68230 to send and receive data over the VXI Local bus (via U11) to the various 50000B modules in the system. U13 also provides the control signals such as address data strobes and Direction strobe to control the Data bus. U9 supplies address decoding for U13. U10 provides the DTACK signal for the operation of U13.

3.6.2 110 MHz Assembly (A101A1)

110 MHz Phase Lock Loop

The function of this circuit is to phase lock the 110 MHz VCO on the oscillator/multiplier board to the 10 MHz master reference. In addition, this circuit performs important functions related to the master reference itself.

The output frequency of the 110 MHz VCO is received at J8 and U2 divides the input by 11. When the loop is locked, the input is exactly 110 MHz, and the divider output is exactly 10 MHz. One output from U2 is applied to the variable input of the phase comparator at U5-9. The other is buffered by U1C and serves as the 10 MHz reference signal out of the 52000B front panel. The reference input to the phase comparator comes from the 10 MHz input/output circuit.

The reference input to the phase comparator U5-6 comes from a switching circuit, which selects either an internal or external 10 MHz reference. When no external reference is present at J12, the internal 10 MHz reference at J10, buffered by U1B, propagates through U4C and the phase comparator (U5-6). When an external 10 MHz signal is present at J12, it is buffered by U1A and propagates through U4A to the phase comparator. The presence of an external 10 MHz reference is detected when a charge is built up on C24 and the switching circuit (comparator U8) switches to a high state. This causes U6 output to go high and turn off the supply to the internal 10 MHz reference. The switching circuit enables the external reference path at U4A and disables the internal reference at U4C. The selected reference is then available through Q3 and Q4 as the 10 MHz (Timebase) reference output on the 52000B front panel.

When its reference and variable inputs are not in phase, U5 produces wide pulses at one of its outputs, depending on whether the variable input is leading or lagging the reference. The pulsed outputs are filtered and amplified by U3-7 to produce a voltage output (J11) which tunes the 110 MHz VCO.

The lock indicator circuit (U3-1, Q1) responds to the wide pulses that occur on the phase comparator outputs when the loop is unlocked. The lock indicator turns on Q1, pulls the output low and turns on DS1. When the loop is locked, Q1 and DS1 are off.

3.6.3 110 MHZ Oscillator/Multiplier Assembly (A101A2)

This circuit is the source for the 220 MHz and 330 MHz reference signals used by various phase lock loop circuits in the Synthesizer.

The voltage controlled crystal oscillator (Q1, etc.) uses a quartz crystal resonator (Y1). A tuned circuit (L2, etc.) restricts the crystal to an oscillation mode at 110 MHz. The VCXO is fine tuned by a voltage input from the 110 MHz PLL circuit (A12). Its output signal is amplified by AR1 and buffered by line receiver U1. The buffered 110 MHz signal is fed back to the PLL and is also furnished to the frequency tripler.

The frequency tripler takes advantage of the powerful third harmonic component present in any square wave. The U5 line receivers produce a square 110 MHz signal, which is inductively coupled through a band-pass circuit (L4/L5, etc.). C17 and C18 provide peaking adjustment. Two band-stop filters on the output (L3, L6) remove the fundamental and the second harmonic of the VCXO frequency. The 330 MHz output is not buffered because the circuit to which it is furnished does not require a high power input.

3.7 Detailed Circuit Descriptions (Synthesizer)

3.7.1 Decode/DDS Assembly (A1)

This assembly contains the decode circuitry, which controls the 80 MHz Phase Lock Loop, and the Direct Digital Synthesis (DDS) circuitry.

Address Decode

This circuitry provides address decoding for the whole Synthesizer module. This module is controlled by the 52000B Control module via the 12 Local Bus lines available on the VXI Bus. Of the 12 available lines, 8 are used for the data bus, one to simulate an Address strobe, one for a Data strobe, and another line for Direction or read/write line.

Bidirectional buffer U5 buffers input from the Local bus and the LDIR line controls direction of the data or address being read or written.

To address a specific chip in a particular module and board, the first set of data written to this board from the control module consists of a module address and a chip address. The chip address bits (0-3) are used by the U6 decoder to decode the specific chip to be read from or written to. The module address bits (4-6) are used by decoder IC U4 to decode the module address. If the decoded module address matches the address selected by the switch at SW1, it enables the LDS and LAS (Local data and address strobes) to propagate thru U1, thus latching the desired chip address at U6 and the selected module address at U4.

Depending if the function is to read or write, the LDir line selects the direction of the U5 buffer. When the LDS or data strobe is received the data is read from the selected chip or written to the selected chip.

U8 is selected when CS0 is activated. This latch allows the module type to be read to identify the module as a synthesizer. The U9 latch allows the status from various PLLs and the leveling loop to be read. U10 decodes the various PLL lock signals to drive the front panel Lock LED. U11 provides control signals for the Reset PROM on A2. Some of the chip selects generated at U6 go directly to circuits on A1; however, many others go to A2 and A3 via the P3 connector.

80 MHz Oscillator and PLL

This circuit generates an 80 MHz reference signal for the DDS chip. The PLL circuitry phase locks the 80 MHz VCO to the 10 MHz reference signal. The main elements of the circuit are the voltage controlled oscillator (VCO), the divider, the phase comparator, and the lock detector.

The VCO (Q2, etc.) oscillates around 80 MHz; its output frequency is determined by the tuning voltage received from U14-1. The VCO output is furnished to the DDS chip after being buffered by Q3 and Q5. The VCO output is also divided by 8 at U13 and applied to the input of the phase comparator (U15-6).

The phase comparator produces pulses at one of its output pins (U15-3 or U15-12) depending on whether its variable input at pin 9 is leading or lagging the reference input at pin 6. The 10 MHz input at pin 9 is from J4, which comes from the front panel of the Synthesizer. The U14-A loop amplifier converts U15 output pulses into a DC control voltage for the VCO. The phase comparator tunes the VCO upward or downward in order to equalize its two input frequencies. When these two frequencies are equal, the loop is locked. The phase comparator output pulses are furnished (via CR3 and CR4) to the lock detector circuit (U14-B). When the loop is unlocked (i.e., when there is a large difference between the phase comparator inputs) the output pulses become very wide, U14-7 goes high to turn on Q4 and fault indicator DS1, and pulls the LOCK output low.

80 MHz DDS

The circuitry in this section digitally synthesizes a reference frequency for the instrument's output phase locked loop.

The digital information to program the U20 DDS chip is supplied via latch U18. The control signals to strobe the data into the chip and to identify what information is present in the byte loaded at U18, are provided to the chip from latch U19. The 80 MHz reference clock required by the U20 DDS chip and the U16 D/A converter is amplified to CMOS levels via Q6, Q7, and U21-F, and then buffered by the remaining sections of U21 before being supplied to the U20 DDS chip.

Sections A, B and C of U21 can be jumpered to provide different delays of the 80 MHz clock before it is supplied to D/A U16. Coils L11-13, and associated capacitors create a 20 MHz low pass filter to filter harmonics and other spurious signals from the 2 to 20 MHz signal created by the DDS/DA combination. This 2 to 20 MHz signal is buffered by U17 and shifted to ECL levels before being made available to the output PLL at J5.

3.7.2 Level/RF Control (A2)

This assembly contains the Reset ROM, Level Control circuitry, and the Output and 300 MHz PLL. It also provides power, chip selects and data bus lines to the Driver and YIG Driver PC assemblies (A3 and A4) via the P4 ribbon cable.

The chip selects the control lines and data bus lines from the RF/Decode PCA #1 assembly through the ribbon cable at P3. Latches U2 and U6 allow two 8-bit addresses to be latched to create a 16-bit address to address the U5 Reset ROM for the Synthesizer module. The U5 Reset ROM is programmed with information unique to the Synthesizer; including its hardware characteristics, frequency ranges, level and frequency correction data. The controller module must read this information via U50 before it can control the Synthesizer. U1 latches the various logic states for the level and output loops.

Output PLL and Divider

The output PLL circuitry produces a control signal for use in fine-tuning the instrument's YIG oscillator, in order to phase lock the YIG frequency to the master reference. In the FM mode, the control signal is combined with a modulation input.

The U11 phase detector receives two input frequencies, both in the 5 to 10 MHz range. These frequencies are equal when the loop is locked. The reference frequency input comes from the divide-by-8 circuit on the A1 board (J-46) and the variable frequency input (fV) comes from the programmable divider circuit on this board. The phase detector produces outputs at pins 4 and 18 of U11. If the input frequencies are not in phase, wide pulses appear at one of these pins, depending on whether fV is leading or lagging. The outputs are used by the lock detector circuit (see U48-7, Q1) to determine if the loop is locked. They are also used by one of two independent loop amplifier circuits (selected by analog gate U10) to produce the loop control output.

The first loop amplifier circuit is used when the instrument is not in FM mode. The phase detector outputs are amplified by U9-1 and U9-7. Frequency compensation networks (R25/C22, R20/C21, R14/C18) provide the rolloff needed to stabilize the loop. Diodes in the amplifiers feedback loops limit the amplifier outputs to prevent saturation during the search mode. The output of U9-7 is applied through a driver amplifier. This output tunes the YIG oscillator FM coil; it goes more negative to increase frequency and more positive to decrease.

The second loop amplifier circuit is used when the instrument is in the FM mode. Essentially, it duplicates the first loop amplifier (see U13-1, U13-7) but adds the input FM signal (amplified by U12-1)

to the phase detector output signal. The two signals are combined by U12-7 and applied to analog gate U10.

The variable frequency input to the phase detector is derived from the sampling mixer IF, not directly from the YIG output frequency. The sampler's IF is the product of a harmonic multiplier, and may be derived from the wrong harmonic. In that case the phase lock loop is misdirected, tuning the YIG oscillator in the wrong direction until it reaches its positive or negative rail. To prevent the PLL circuit from becoming stuck in this mode, a search circuit is added, consisting of amplifiers U49-1 and U49-7 to monitor the circuit output and return control voltages to the loop amplifier circuits. When the output becomes too positive (minimum frequency), U49-7 swings to its negative rail, driving the output negative (maximum frequency). When the situation is reversed, U49-1 drives the output positive (minimum frequency).

The programmable divider circuit (U16 and U18) is set to divide by 2 in the Series 50000B. It accepts a 6 to 40 MHz sampler IF at J2 from the 300 MHz Oscillator board (A104). A low pass filter (L1, etc.) removes spurious high frequencies from the signal. The logic levels at A & B are fixed at '0'. This takes the divided by 2 output from U16-4), and U17-4 and U17-12 and routes it to D & E phase detector.

300 MHz Phase Lock Loop

This circuit tunes the 300 MHz voltage controlled oscillator (A104 module). The VCO can be programmed over a range of 284 to 319 MHz; the PLL circuit enables the computer to select the desired VCO frequency and phase lock the VCO to the instrument's 10 MHz timebase. The input at J7 is feedback from the VCO. Because the 284 to 319 MHz input frequency is too high to be counted by the digital circuits used here, the input signal is mixed (see U29) with the 330 MHz reference input (received at J8 and amplified by AR3) yielding an intermediate frequency in the range of 11 to 46 MHz. A low pass filter (L2, etc.) removes the mixer input frequencies. The IF is then amplified (AR2) and applied to the programmable divider.

The purpose of the programmable divider is to divide the 11 to 46 MHz IF down to 1 MHz. The first stage of the divider consists of an 8 bit latch, U20; the computer selects the divisor (in the range of 11 to 46). The outputs of the latch are applied to the comparators of U24 and U21; the comparator outputs translate the eight-bit divisor into ECL levels for use by the high speed ECL down-counters, U25 and U22. The counters are clocked by the amplified IF, and count down from the numbers programmed into them. U22 represents the four least significant bits, U25 the four most significant bits. Flip flop U26, also clocked by the IF, receives a high at its D input (U26-13) at the end of the count and sends a high output pulse (from U26-19) to the phase comparator U28. The counters are reset by U26-18 and the count repeats.

The phase comparator chip, U28, requires reference and variable frequency inputs. The reference input is derived from the instrument's 10 MHz timebase. The 10 MHz input is received at J6, filtered (L3, etc.) and divided by ten at U31. The 1 MHz quotient is applied to the comparator at U28-9. The variable input, received from the programmable divider circuit (see U26-19), is applied to the phase comparator at U28-13. The phase comparator produces wide pulses at one of its outputs (pin 4 or 18) depending on whether the variable input is leading or lagging the reference. The loop amplifier circuit (U27, etc.) converts these pulses into a DC voltage output (J5) with which to tune the VCO. The polarity of tuning is: more positive to increase frequency, more negative to decrease frequency. The PLL circuit tunes the VCO in whatever direction will reduce the phase difference between the reference and variable inputs to the phase comparator. Filter components in the loop amplifier circuit (C50, C57, etc.) remove the phase comparator's output pulses from the tuning signal.

When there is a large phase difference between the reference and variable inputs to the phase comparator (i.e., when the loop is unlocked, wide low-going pulses appear at one of U28's outputs. These pulses are detected by the circuit consisting of U30, etc., and cause the LOCK output to go low and the LED (DS2) to be lit. When the loop is locked, U28's output pulses become extremely narrow and shallow, the LOCK output is high, and the LED is extinguished.

Automatic Level Control (ALC)

The ALC circuit drives the leveler, a variable attenuator circuit in the RF module, in order to make fine adjustments of output power. Feedback from a level detector in the RF path is compared with a leveling reference, and the leveler is driven so as to equalize these two inputs. The leveling reference is set by the computer through programming of the digital to analog converter, U34. At U35-6, the reference is combined with a correction voltage from the temperature compensation circuit on A3. During operation in the AM mode, these inputs to U35-6 are also combined with a modulation signal. The AM input is processed by logarithmic amplifier (U39) to match it to the log characteristic of the level reference and temperature compensation inputs) and furnished through U37 to the summing junction at U35-6 (U37 is switched off when AM is off). The combined leveling reference signal is processed by anti-logarithmic amplifier U36 and applied to U47-6, where it is combined with the amplified signal from the level detector (see U40, U42). In the event that the unit has analog power sweep capability, the power sweep ramp signal at J12 will also be summed, via U37, with the other signals at U35 pin 6.

The signal at the inverting input U47-6 is integrated (U47-7) and furnished to the PIN diode leveler circuit in the RF module. The polarity is positive for increased attenuation, negative for reduced attenuation. Following the leveler circuit in the RF path is a level coupler and diode detector. The detector returns a negative voltage proportional to detected RF power. The ALC circuit drives the leveler in such a way that the amplified detector signal and the leveling reference signal cancel for a zero voltage at U47-6.

When the output of U47-7 is within its normal range U46-7 turns off transistor Q6 and the leveled indicator output is pulled high, illuminating the level LED on the unit's front panel. If the ALC circuit has not yet adjusted the RF output to the requested level, a significant voltage will be present at U47-6, turning Q6 on and pulling the indicator output low.

3.7.3 YIG Driver/Temperature Compensation Assembly (A3)

This circuit controls the current source for the tuning coil in the output YIG oscillator. The oscillator tuning coil has a sensitivity of 20 MHz/mA. The computer coarse-tunes the YIG through its programming of this circuit.



NOTE: The components surrounded by a dotted line on the schematic diagram are not located on this circuit board, but are shown for clarity.

U2 is a D/A converter. Its analog output is proportional to the binary number with which it is programmed by the computer. The DAC, together with U1-6 inverting amplifier, furnishes a computer-controlled voltage to the summing junction at U3-2 (by way of the R5 MIN calibration pot). The other inputs to this junction are (1) a negative voltage from reference diode VR1 (by way of the R14 MAX cal pot), (2) a positive voltage fed back from the YIG oscillator tuning coil, and (3) a sweep ramp input from the analog sweep module (during analog sweep operation). The output at U3-6 is furnished by way of Q1 to the base of the transistor which controls the YIG tuning coil current. The computer adjusts the YIG frequency through the programming of the DAC. When the input voltage to amplifier U3-2 changes, its output swings in whatever direction will yield a complementary change in the feedback from the YIG coil, thus maintaining virtual ground at the summing junction.

The U5 analog switches select different operating modes. During sweep operation, a ramp input is received at J1 and inverted by U4-6. The YIG ramp input directs the switching of U5-11 to furnish the signal to the summing junction at U3-2.

During repetitive sweeping, it is necessary to retune the YIG oscillator to the start frequency at the beginning of each sweep. Because the filter capacitors in the circuit resist rapid frequency changes, it is necessary to switch them out of the circuit during the transition. When the FAST line goes high, C12 is grounded through U5-15 and, at the same time, C31 is grounded through U5-7.

The Temperature Compensation circuit provides correction signals in response to internal temperature changes in the instrument. U9 is a temperature sensor, producing an output voltage proportional to temperature. The sensor voltage, amplified by U8-1, is furnished to a circuit consisting of U8-7, CR2, CR3, etc., which provides a correction signal to the level control circuit (A2). This correction signal is required because the sensitivity of the level detector changes with temperature, and this would cause a level error if not compensated. Each detector has a unique temperature response. During production testing, R35, R36 and R37 are selected and the ZERO pot (R33) is adjusted to match the response curve of the instrument's particular detector. **THESE VALUES SHOULD NOT BE CHANGED.**

3.7.4 Attenuator/Pulse Driver Assembly (A4)

The Driver circuitry provides harmonic filter selection and pulse modulation of the output signal. The pulse modulation is applied to the switching diodes of the harmonic filter network. An unmodulated filter system is used for the reference channel of the Synthesizer.

Decoder U1 selects the filter used in the reference channel. The TTL level low true outputs of the decoder are buffered by various amplifiers to provide a bipolar drive of about $\pm 5V$ to the filter module.

A second decoder, U2, selects the output filter ranges. In this case, the pulse modulation signal is applied to the enable pin. Once selected, the external pulse, clamped by CR3 and CR4, is routed to U2 pin 4 via U4A.

Each decoder output has a two-transistor driver to convert the TTL levels of the decoder to the ± 5 volts required by the filter module. Resistor and capacitor values are chosen to optimize the pulse rise/fall time.

Attenuator Relay Driver

The 10 dB step attenuator is programmed to switch any or all of four fixed-attenuation segments into or out of the device's RF path. The attenuation values of the individual segments are 30 dB, 30 dB, 20 dB and 10 dB. For a setting of 90 dB, all segments are activated. The mechanical switching is enabled by relay drivers, U11 and U12, which respond to TTL-level inputs and provide output levels of zero and approximately +24 volts. By programming the drivers, the computer can select attenuation values between zero and 90 dB, in steps of 10 dB. U14 allows the filter select lines to be controlled from the sweep module during analog sweep.

3.7.5 VXI 10 MHz Buffer Assembly

This circuit receives a 10 MHz input at J5 from the front panel 10 MHz input connector (the source of this signal is the Control module or another Giga-tronics module). The 10 MHz reference signal is buffered by U1 and supplied to several other circuits (via J7, J8, and J9) and to the front panel 10 MHz output connector (via J6).

3.7.6 VXI 330 MHz Buffer Assembly

This circuit receives a 330 MHz input (at J1) from the front panel 330 MHz input connector (the source of this signal is the Control module or another Giga-tronics module). The 330 MHz reference signal is buffered by U3, U4, U5, and U6 and supplied to the 300 MHz PLL (A2) (via J3), and to the front panel 330 MHz output connector (via J2).

3.7.7 300 MHz Oscillator/Driver Assembly (A104)

This circuit board is encased in an aluminum housing and mounted directly beneath the RF module; it is not normally accessible to service in the field.

The tuning output from the 300 MHz PLL circuit on A2 is received at J2. A 1 MHz trap (L3, etc.) reduces the reference-frequency component contributed by the PLL's phase detector. The filtered control signal is applied to the voltage-controlled oscillator (Q4). A sample of the VCO frequency is fed back to the PLL circuit (see AR2) in order to permit phase lock. The VCO operates over a range of 283 to 319 MHz.

The VCO output frequency is taken at L2; this inductor is implemented as a conductive strip in the printed circuit artwork and is tapped very close to ground in order to reduce the load on the oscillator and insure stability. The VCO frequency is amplified by AR1 and AR7 to meet the input level requirement of the sampling mixer (about 4 V_{p-p}).

The sampling mixer is a miniature hybrid RF circuit which combines a mixer with a step-recovery diode multiplier. The multiplier (to which the VCO frequency from the driver is applied) generates numerous harmonic multiples of its input frequency. The harmonics are used as one input to the RF mixer; the other input (see J4) is a sample of the YIG oscillator frequency, obtained from a coupler in the RF module. Because one mixer input is a harmonic series, the intermediate frequency output includes numerous sum and difference frequency components.

The mixer IF must be filtered and amplified in order to isolate one IF component in the range of 10 to 80 MHz. The power level of the IF output is very low; AR3, AR4 and AR5 each provide about +19 dB of gain, and the final amplifier stage (AR6) provides about +33 dB of gain. Three low-pass filters (L6, L8 and L11) roll off sharply above 130 MHz to eliminate harmonics of the IF. The amplitude of the sampling mixer IF is highly variable with frequency; in order to obtain a flat frequency response, an AGC circuit is added (U2-7). Diodes CR4 and CR5 are used by the circuit as signal level detectors; a correction voltage is produced and is applied to attenuator diode CR3 in order to maintain a 1 V_{p-p} IF output at J3.

Calibration & Testing

4.1 Calibration Procedure

- The instrument being calibrated or tested is referred to in these procedures as the UUT (Unit Under Test)
- The required warm-up time before calibration or testing is 30 minutes
- Calibration tolerances referred to in these procedures are intended to optimize the performance of the UUT; they should not be construed as specifications. Performance specifications are presented in Chapter 1 of the manual. The recommended interval between calibrations is one year

4.1.1 Required Test Equipment



NOTE: *Equivalent equipment may be substituted*

VXI Mainframe – Tektronix VX1400
VXI 0 Slot controller – Tektronix VX4530
Giga-tronics 52000B Control Module
Oscilloscope – Tektronix 2465A
Microwave frequency counter – XL Microwave 3260
Power meter – Giga-tronics 8541

Power sensor – Giga-tronics 80303
Function generator – Agilent 3312A
Detector – Krytar 201S
Spectrum analyzer – Agilent 8566B
FM test fixture (Discriminator) – Giga-tronics
Modulation meter – Wavetek 4101

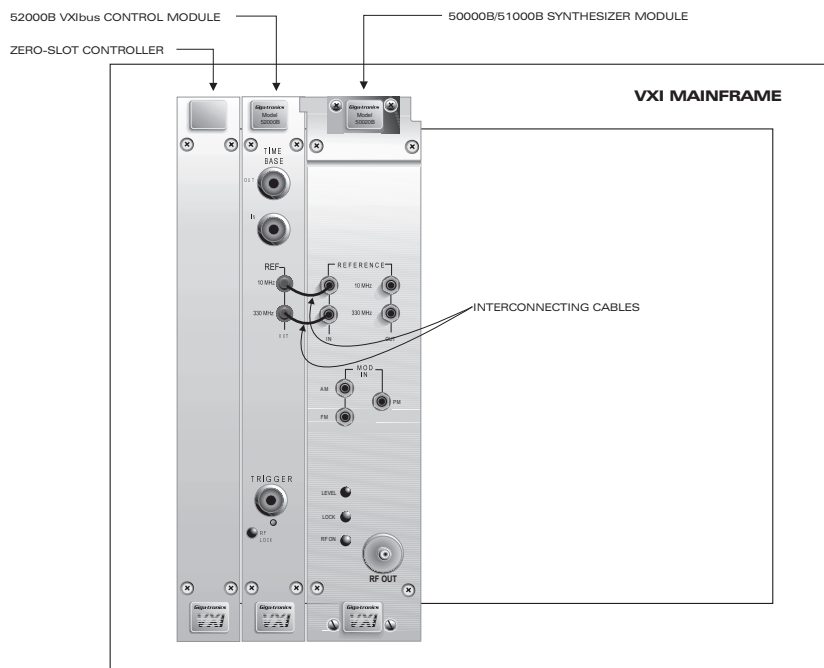


Figure 4-1: Typical Series 50000B Setup

4.1.2 Timebase Calibration

Use the following steps to adjust the timebase of the Model 52000B Control Module:

1. Connect a microwave frequency counter to the UUT RF output connector. Connect the counter timebase to a known accurate standard.
2. Set the UUT to its highest frequency of operation at 0 dBm.
3. Carefully adjust the UUT timebase adjustment(s) for a counter reading equal to the UUT setting.

4.1.3 YIG Driver

Use the following steps to adjust the YIG driver (A3) in the Model 50XXXB Synthesizers Module:

1. Monitor the PLL drive (available on a 2 PIN connector on the "Regulator/FM Driver" board. This board is near the YIG oscillator) with an oscilloscope.
2. Set UUT to max RF frequency. Adjust R14 (A3) MAX pot for an oscilloscope reading of $+1.5 \pm 0.5$ V.
3. Set UUT to min frequency (not including downconverter range). Adjust R5 (A3) MIN pot for an oscilloscope reading of $+1.5 \pm 0.5$ V.
4. Repeat steps 2 and 3 as needed.

4.1.4 Level Calibration



NOTE: If it is necessary to adjust the reading more than 1dB with the -4 pot, the linearity of the AM may be affected. Use the +4 pot to achieve the best compromise at both +4 dBm and -4 dBm while adjusting the -4 pot as little as possible.

1. Connect a power meter to the UUT RF output connector.
2. Set the UUT to a mid-range frequency at a power level of +4 dBm.
3. Adjust the R117 (A2) +4 pot for a reading of +4 dBm on the power meter.
4. Set the UUT to -4 dBm and adjust the R161 (A2) -4 pot for a power meter reading of -4 dBm.
5. Repeat steps 3 and 4 as needed.
6. Verify the level flatness and accuracy at various frequencies and power levels.

4.1.5 AM Calibration

In many places, this procedure refers to measurements made by using a spectrum analyzer as a downconverter to feed a modulation meter. The procedure will work equally well with a variety of analyzers and modulation meters. Some other form of downconverter can also be used. In all cases, be certain that no amplitude compression nor distortion is introduced by the measurement system.

1. Connect the UUT's RF OUT to the spectrum analyzer. Connect the IF output from the spectrum analyzer to the input of the external modulation meter.
2. Set the UUT to a mid-range output frequency, at +3 dBm with all modulation off. Set center and top reference level on the spectrum analyzer, span 500 kHz, center and top reference level.
3. Monitor Test Point 3 on the A2 board with the DVM (2V scale), and adjust the Zero pot (R150) on that board for a reading of zero volts dc.
4. Connect a function generator set at 1 kHz at 1 Vpp to the AM MOD input on the UUT. Turn EXT AM on. Set analyzer to zero span (time domain), linear vertical display, sweep time 10 ms, increase the reference level to get the display on the screen. Adjust the AM pot (R132) on the A2 board for an external modulation meter reading between 49% and 51%.

4.1.6 FM Calibration

A special test fixture must be assembled to calibrate and test the frequency modulation circuits (see Figure 4-11). The recommended FM test fixture includes an RF splitter, two lines of unequal length, and an RF mixer. The RF output of the UUT is divided by the splitter into two signals, unequally delayed. The required differential delay can be obtained by using two coaxial cables of, for example, 5 and 10 inches in length. The outputs of these delay lines are furnished to the two inputs of the RF mixer. For certain frequencies which may be identified by experiment, the mixer will produce a dc voltage near zero. The number of null frequencies can be increased by making the delay lines longer in absolute terms or by increasing the ratio between their lengths. If the output becomes frequency modulated, the mixer output voltage will change, and the voltage variation will be proportional to FM deviation. The polarity of the voltage change may be either directly or inversely related to the direction of frequency deviation. When voltage levels have been established for different frequencies, the mixer output can be monitored on an oscilloscope to provide a continuous display of FM deviation.

1. Connect the FM test fixture to the RF OUT connector of the UUT. Monitor the mixer output with the oscilloscope (5 mV/div). Set the UUT to a null frequency (that is, at a frequency where the mixer output voltage is zero); +5 dBm out; no modulation.
2. Establish the voltages at 5 MHz above and 5 MHz below the null frequency. Adjust the oscilloscope gain and the UUT output power level (near +5 dBm) to place the null point at the center of the screen and the 5 MHz deviation points at 3 divisions above and 3 divisions below the null point.
3. Connect a function generator set to 1 kHz at 2 Vpp to the FM MOD input on the UUT. Turn on EXT FM. Adjust the FM CAL pot (R34) on the A2 Output PLL to make the mixer output six divisions peak to peak.

4.2 Performance Tests

The procedures listed in this section are used to verify the electrical performance of the Series 50000B, using the specifications of Chapter 1.

When an adaptor module (such as the Scan Modulation module) is present, that module's RF output becomes the Series 50000B or System RF output; specifications for these modules are described in Chapter 1.

4.2.1 Equipment Required



NOTE: *Equivalent equipment may be substituted*

Microwave Frequency Counter – XL Microwave 3260

Microwave Spectrum Analyzer – Agilent 8566B

Local Oscillator – Giga-tronics 6100

Power Meter – Giga-tronics 8541

Power Sensor – Giga-tronics 80303

Measuring Receiver – Agilent 8902A

Downconverter Mixer/IF Amp – Giga-tronics, see Section 4.2.10

Plotter* – Agilent 7470

Computer* – MS-DOS with IEEE interface

Oscilloscope – Tektronix 2465A

Crystal Detector – Krytar 201S

Digital Voltmeter – Fluke 8012A

Function Generator – Agilent 3312A

FM Test Fixture (Discriminator) – Giga-tronics, see Section 4.2.11

* Required for automated tests only.

4.2.2 Test Data Sheet

A Test Data Sheet is included to allow entering the various readings taken. The specification and tolerance range is listed to allow ease of verification. It is suggested that copies be made of the manual sheets.

4.2.3 Frequency Range, Resolution, & Accuracy

Specifications

Range:	Determined by the model number
Resolution:	1 Hz
Accuracy:	Same as timebase accuracy

Description

The output of the Series 50000B is connected to the input of a frequency counter. The internal time base of the Series 50000B is used as a reference for the counter to eliminate time base errors from the measurements.

It is possible for a fault in the synthesizer to cause frequency errors even though the lock indicators show normal operation (in other words, it is possible for the synthesizer to fail in such a way that it becomes locked on the wrong frequency). For this reason, a number of specific frequencies are tested; test frequencies have been selected so that any defective circuit can be readily isolated.

Equipment Required

Frequency Counter • Coaxial Cable • SMA to Type N Adapter • SMA to Type BNC Adapter

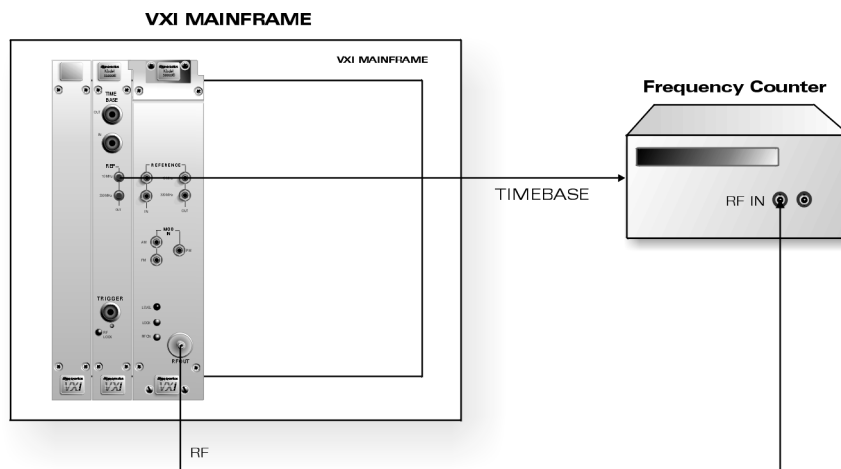


Figure 4-2: Frequency Range, Resolution & Accuracy

Procedure

1. Connect the equipment as shown in Figure 4-2. Allow the equipment at least 30 minutes of warm-up. Since the Series 50000B and the counter use the same time base, time base errors are eliminated.
2. (Skip this step if the Series 50000B does not include the Downconverter range). Enter **[CW] [1] [0] [Mz]**. Enter **[PL] [-] [1] [0] [dB]**. The counter should read 10 MHz \pm 1 Hz \pm the counter resolution.
3. If necessary, connect the RF Out to the counter 500 MHz-18 GHz input. Enter **[CW]** and then the maximum frequency. The counter should read the entered frequency \pm 1 Hz \pm the counter resolution.
4. To check that the various PLL circuits are functioning properly, refer to the Test Data Sheet and program each of the available listed frequencies into the Series 50000B by entering (for

example) **[CW] [2] [0] [0] [0] [Mz]**. For each listed frequency the counter should read the entered frequency $\pm 1 \text{ Hz} \pm$ the counter resolution.

5. This test exercises the 1 Hz through 100 kHz digits in such a manner that any incorrect digital programming data being sent to the 1 Hz Resolution assembly will be detected. Improper operation of the 1 Hz assembly itself will likewise be indicated. Refer to the Test Data Sheet and program each of the listed frequencies into the Series 50000B.

4.2.4 Spurious Signals Tests

Specifications

Harmonics (up to maximum frequency of synthesizer):	<-50 dBc, 2 - 20 GHz; <-40 dBc, 0.01 - 2 GHz (with Downconverter)
Sub-harmonics:	None
Non-harmonics:	<-40 dBc <100 kHz offset <-50 dBc 100 kHz - <1 MHz <-60 dBc >1 MHz

Description

The output of the Series 50000B is connected to a spectrum analyzer. Various frequencies are selected and the analyzer tuned to determine the presence of either harmonic or non-harmonic spurious signals.

Equipment Required

Spectrum Analyzer • Coaxial Cable

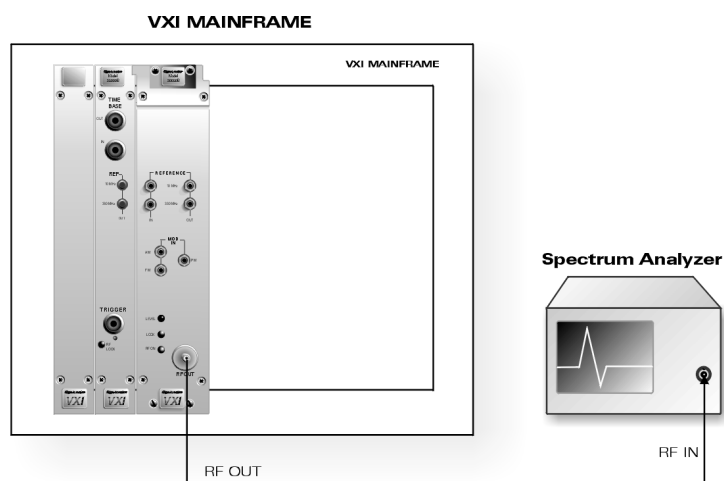


Figure 4-3: Spurious Signals Tests

Procedure

1. Connect the equipment as shown in Figure 4-3. Enter the first Test Data Sheet frequency which is within the range of the particular instrument. The RF amplitude should be at +0 dBm for harmonic tests and 0 dBm for spurious.
2. Set the spectrum analyzer to view the Series 50000B output signal. Adjust the analyzer reference level such that the peak of the displayed signal is at the top graticule line.

Many spectrum analyzers have a tuned preselector when the frequency is above about 2 GHz. This reduces the likelihood of analyzer generated spurious signals, but does not eliminate the possibility. If in doubt, increase the RF Attenuation of the analyzer by 10 dB. The signal in question should be reduced by exactly 10 dB. If not, it is analyzer generated. It is also important, for frequencies below the range of the preselector, that sufficient analyzer RF Attenuation be used (typically 30 dB) to avoid the analyzer generating harmonics of the input signal. The above attenuator shift technique will also allow verifying harmonic levels.

3. If a spurious signal appears to be out of specification, first verify that the fundamental signal level is at 0 dBm. Next verify the analyzer accuracy by connecting a known amplitude signal (from the Series 50000B, for example) at the spurious frequency.

The acquisition of the various phase lock loops in the instrument can cause transients (within the specified settling time). These effects will disappear when a steady state condition has been reached.

4. Set the spectrum analyzer to a span of 50 Hz per division with the signal centered on the screen. Gradually increase the span to allow observing any spurious signals. Use appropriate resolution and video bandwidths to allow sufficient dynamic range.

It is important to identify the particular class of spurious signal as the specifications may be different for each. If the spurious is an exact multiple of the Series 50000B RF Output then the harmonic specification applies.

There are no sub-harmonics in the Series 50000B as all frequencies are fundamentally generated (or mixed, if below 2 GHz). Any other spurious signal must meet the non-harmonically related specification.

5. Repeat steps 2 and 3 for the other frequencies on the Test Data Sheet which are within the operating range of the instrument.

4.2.5 Single Sideband Phase Noise

Specifications

See the SSB Phase Noise specification on page 1-6.

Description

The output of the Series 50000B is connected to the spectrum analyzer. Various frequencies are selected and measured.

Equipment Required

Spectrum Analyzer • Coaxial Cable

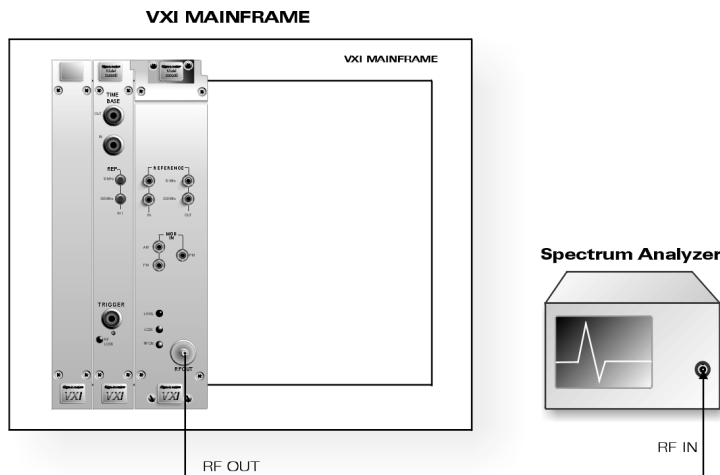


Figure 4-4: Single Sideband Phase Noise

Procedure

1. Connect the Series 50000B RF Output to the spectrum analyzer input.
2. For the first frequency on the Test Data Sheet which is within the range of the instrument, enter the frequency. Tune the spectrum analyzer to the generator frequency and adjust the Series 50000B RF Level to obtain a reference of 0 dBm on the analyzer. This allows direct measurement of the phase noise by the analyzer.
3. Set the analyzer span such that the desired offset is at ± 2 divisions, select an appropriate bandwidth, activate the phase noise measurement and place the marker two divisions above the carrier. Read the phase noise in dBc/Hz.
4. Repeat 2 and 3 for the other Test Data Sheet frequencies which are within range of the instrument under test.

4.2.6 RF Output Power Tests

Specifications

Maximum Levelled Output:	$\geq +8$ dBm (.01 - 2 GHz) $\geq +12$ dBm (2 - 12 GHz) less 1 dB 8 - 16 GHz and 2 dB >16 GHz with Option 26 $\geq +9$ dBm (12 - 20 GHz) less 1 dB 8 - 16 GHz and 2 dB >16 GHz with Option 26
Minimum Output Level:	-90 dBm (with Option 26) -10 dBm (without Option 26)
Level Accuracy:	± 2 dB
Level Flatness:	Included in accuracy

Description

Although it is possible to make the following measurements manually, it is extremely tedious. It is recommended that an automated system be set up to take and record the data. Three tests are run. The first measures the maximum available output with the instrument leveling disabled. The second verifies the accuracy and flatness across the operating frequency range at a fixed output (0 dBm). The remaining test checks the step attenuator accuracy at a number of frequencies. The procedure outlines the general procedure followed by the automated system. A similar measurement can be done manually.

Equipment Required

Local Oscillator • Power Meter & Sensor • Measuring Receiver • Downconverter mixer/II • Plotter • Computer & Programs

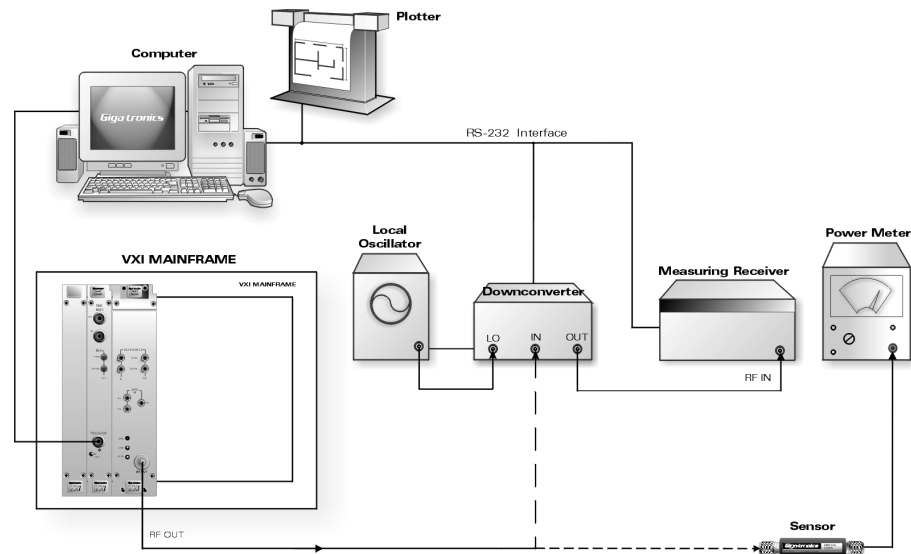


Figure 4-5: RF Output Power Tests

Procedure

1. Connect the power meter sensor to the UUT. Disable the leveling system of the UUT by disconnecting J10 on A2. Step the frequency across the particular instrument operating range in 50 MHz increments. At each point measure the power, apply the appropriate sensor correction factor, and plot the result.
2. Using the above setup, set the UUT to 0 dBm with the leveling enabled. Again step the frequency across the operating range, measure, correct and plot the power.
3. Connect the UUT to the measuring receiver via the downconverter. With the UUT at 0 dBm and set to the first test frequency, establish a reference on the receiver. Reduce the UUT output in 10 dB steps, observing and recording the receiver reading. As needed, perform the recalibration requested by the receiver. Repeat for the remaining test frequencies.

4.2.7 Pulse Modulation On/Off Ratio Test

Specifications

On/Off Ratio: >80 dB

Description

The Series 50000B is set to a CW frequency at a power level of 0 dBm. A spectrum analyzer is used to view the signal. The pulse modulation is then enabled and the resulting waveform is measured.

Equipment Required

Spectrum Analyzer • Coaxial Cable • Function Generator

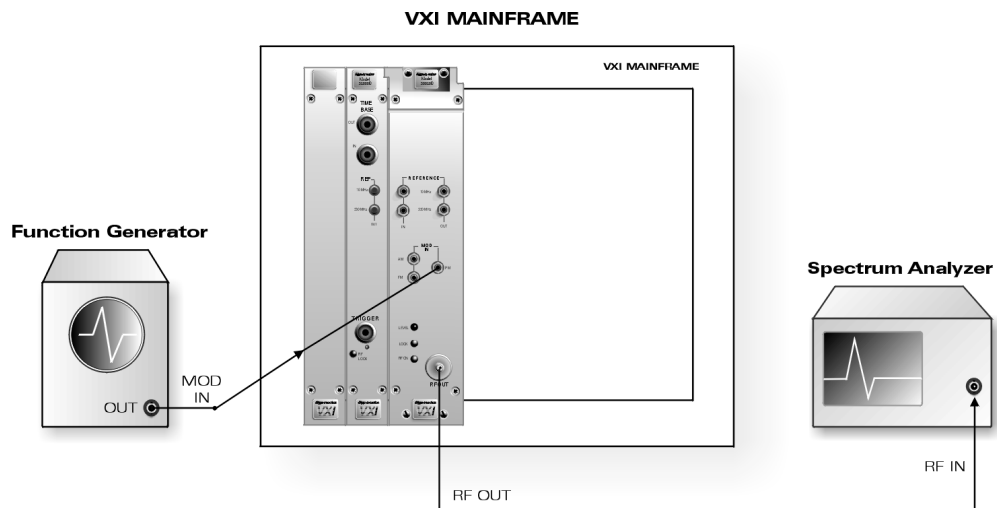


Figure 4-6: Pulse Modulation On/Off Ratio Test

Procedure

1. Connect the equipment as shown in Figure 4-6.
2. Enter the first frequency on the Test Data Sheet which is within the frequency range of the instrument. The RF power level should be at 0 dBm.
3. Tune the analyzer to the source frequency, select an analyzer span of 0 Hz, and fine tune the analyzer to place the line at the top of the screen graticule (adjust analyzer reference level as needed).
4. Connect an external TTL level pulse source at a 100 Hz rate (squarewave) to the PM MOD input. Turn PM on.
5. Adjust the analyzer sweep time to display a few cycles of the waveform. Use video triggering. Reduce resolution bandwidth and carefully retune the analyzer center frequency until the maximum resolution is achieved. Read and record the peak-to-peak value (use marker delta).
6. Repeat steps 3 - 5 for all other Test Data Sheet frequencies which are within the range of the instrument.

4.2.8 Pulse Modulation Rise & Fall Time Test

Specifications

Rise/Fall Time: <25 ns

Description

A crystal detector is connected to the Series 50000B, terminated into 50 Ω , and monitored with an oscilloscope.



NOTE: It is very important to use the specified detector or one with similar rise time characteristics. Even when terminated into 50 Ω with a short cable, the detector parameters can markedly influence the measurement.

Equipment Required

Oscilloscope • Crystal Detector • Function Generator

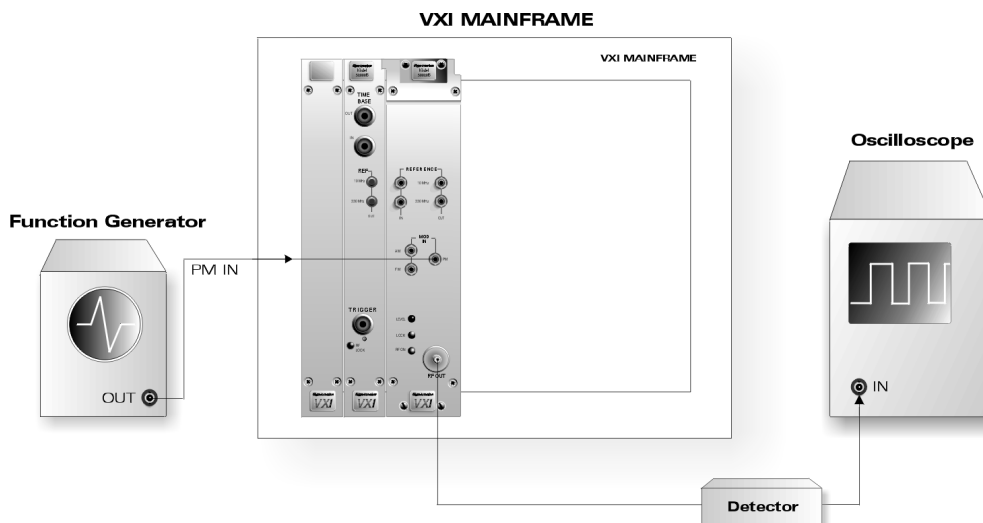


Figure 4-7: Pulse Modulation Rise & Fall Time Test

Procedure

1. Connect the equipment as shown in Figure 4-7. The cable from the detector to the oscilloscope should be kept as short as possible.
2. Set the frequency to the first Test Data Sheet frequency which is within the operating range of the instrument.
3. Connect an external TTL pulse source at a 1 MHz rate (squarewave) to the PM MOD input. Turn PM on.
4. Set the oscilloscope to 5 mv/div and using the RF Level Control of the Series 50000B, adjust the peak to peak oscilloscope display to fall on the dotted lines on the screen (100% and 0%). Adjust the oscilloscope sweep time to 5 ns/div. Measure and record the rise and fall times between the 10% and 90% points.
5. Repeat step 4 for each of the Test Data Sheet frequencies which is within the operating range of the instrument.

4.2.9 Pulse Modulation Overshoot

Specifications

Overshoot, Undershoot,
Ringing: $<\pm 2$ dB, typical

Description

A crystal detector is connected to the Series 50000B, terminated into 50 Ω , and monitored with an oscilloscope.



NOTE: It is very important to use either the specified detector or one with similar rise time characteristics. Even when terminated into 50 Ω with a short cable, the detector parameters can markedly influence the measurement.

Equipment Required

Oscilloscope • Crystal Detector • Function Generator

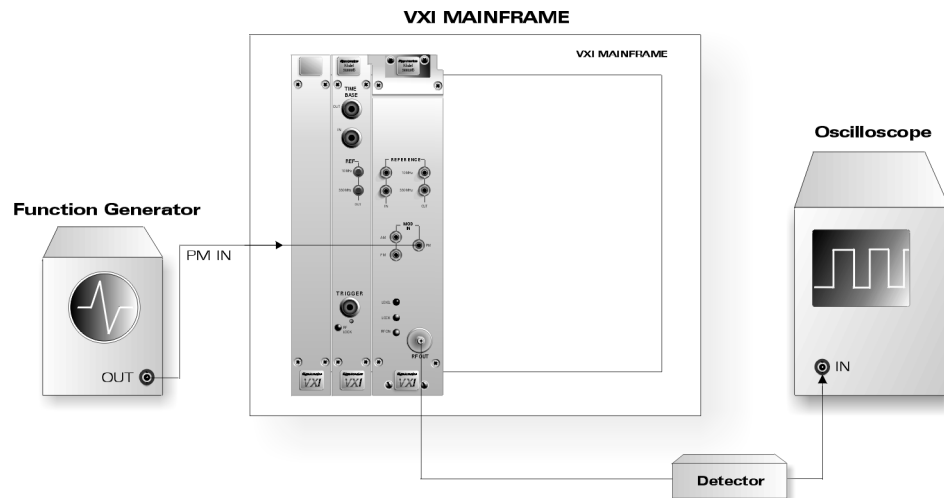


Figure 4-8: Pulse Modulation Overshoot

Procedure

1. Connect the equipment as shown in Figure 4-8. The cable from the detector to the oscilloscope should be kept as short as possible.
2. Set the frequency to the first Test Data Sheet frequency and the amplitude modulation to 0 dBm which is within the operating range of the instrument.
3. Connect an external TTL level pulse source at 1 MHz rate (squarewave) to the PM MOD input. Turn PM on.
4. Set the oscilloscope to 5 mV/div and using the RF Level Control of the Series 50000B and the vertical position of the oscilloscope, adjust the peak to peak oscilloscope display to be from the top of the screen (pulse off) to 2 divisions below the center line (pulse on). Adjust the oscilloscope sweep time to 50 ns/div.
5. Change the level setting of the Series 50000B by plus and minus 2 dB and note the graticule position of the pulse ON level. Return to the original level. Measure and record any undershoot/overshoot of the signal.
6. Repeat steps 4 and 5 for each of the Test Data Sheet frequencies which is within the operating range of the instrument.

4.2.10 Amplitude Modulation Tests

Specifications

Depth:	At least 82%
Bandwidth:	10 Hz to 10 kHz @ 3 dB points referenced to 1 kHz (measured at 50%)
Harmonic Distortion:	10% max @ 50% depth and 1 kHz rate (measured at 7 dB below max power)
Sensitivity:	1 V _{p-p} = 50% modulation $\pm 10\%$ (i.e., 40% to 60%) at a 1 kHz rate, measured 7 dB below maximum power

Description

The output from the Series 50000B is mixed down to a VHF IF and then connected to a measuring receiver. For the modulation depth and accuracy tests, the modulation receiver makes a direct measurement. Modulation bandwidth is measured in the relative mode, referenced to 1 kHz. The internal measurement capability of the measuring receiver is used to measure distortion at 1 kHz. Sensitivity is measured using an external source and RMS voltmeter.



NOTE: Since the measuring receiver is not capable of measurements below 20 Hz, it is not possible to use it to verify performance at 10 Hz.

Equipment Required

Local Oscillator • Downconverter Mixer/IF Amp • Measuring Receiver • Function Generator • Digital Voltmeter

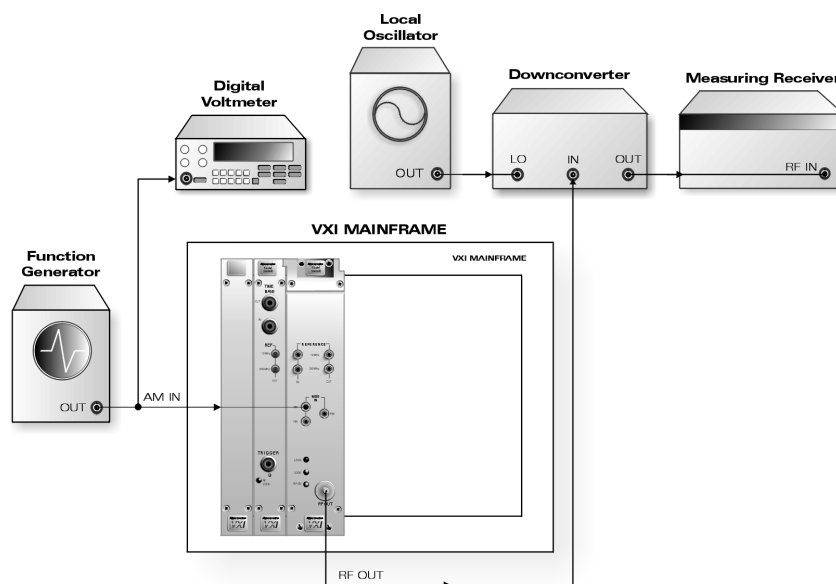


Figure 4-9: Amplitude Modulation Tests

The Downconverter mixer/IF amp specified may be constructed from readily available off-the-shelf components. The mixer must have an RF and LO frequency range at least as great as the generator under test. The mixer IF should be at least 300 MHz. To prevent overload of the mixer, a 10 dB pad is used on the RF port and the LO port is operated at a level of +7 to +10 dBm. The IF amplifier should have about 15 to 20 dB of gain at 130 MHz and a bandwidth not exceeding 300 MHz.

Procedure

1. Connect the equipment as shown in Figure 4-9. The following steps are to be performed at each frequency on the Test Data Sheet. In each case, set the local oscillator 130 MHz below the test frequency.
2. Set the function generator to a frequency of 1 kHz and (measured with the digital voltmeter in ac mode) an amplitude of $2 V_{p-p}$ (1.414 volts_{rms}). Turn AM on. Set the measuring receiver to AM mode with the 20 kHz high pass filter on. Verify that the modulation depth is at least 82%.
3. Reduce to $1 V_{p-p}$. Read and record the depth on the measuring receiver.
4. Put the measuring receiver in ratio mode, logarithmic. Turn off all the filters on the measuring receiver. Reset the function generator to 1 kHz. Enable the measuring receiver ratio mode. Vary the function generator from 10 Hz to 10 kHz and verify that the bandwidth is within ± 3 dB.
5. Deactivate the ratio mode on the measuring receiver. Set the low pass filter to 300 Hz and the high pass filter to 200 kHz. Set the function generator to 1 kHz. Set the measuring receiver to measure distortion and record the reading.

4.2.11 Frequency Modulation Tests

Specifications

Deviation:	5 MHz peak
Bandwidth:	10 Hz to 1 MHz @ 3 dB point
Sensitivity:	2 V _{p-p} for maximum deviation (nominal)

Description

The output from the Series 50000B is connected to a discriminator. The discriminator output is monitored on an oscilloscope to determine deviation and bandwidth.

Equipment Required

Function Generator • Digital Voltmeter • Oscilloscope • FM Test Fixture

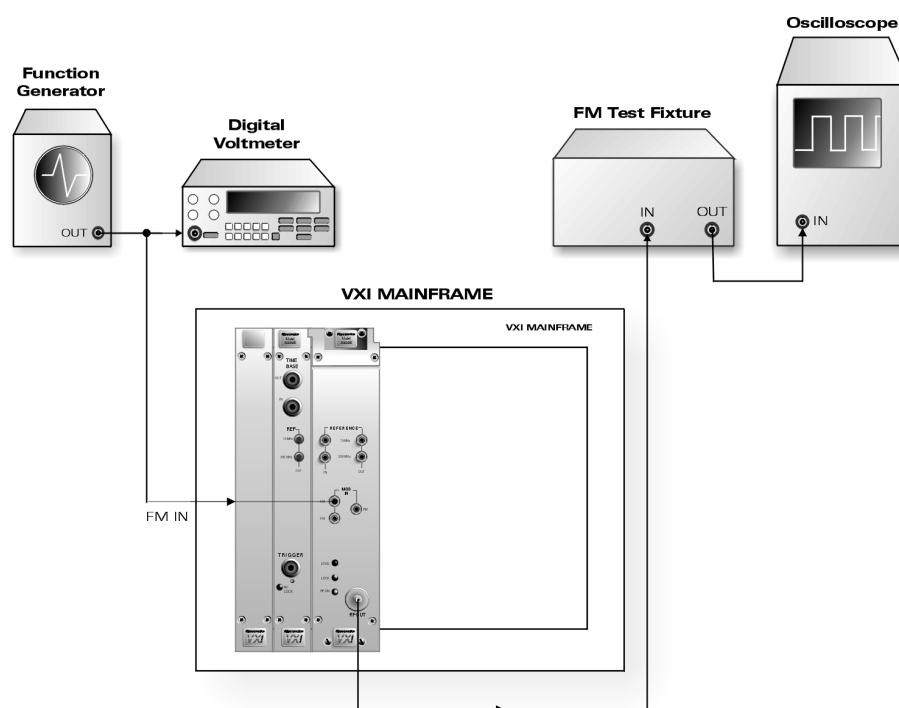


Figure 4-10: Frequency Modulation Tests

Procedure

A special test fixture must be assembled to calibrate and test the frequency modulation circuits. The recommended FM test fixture includes an RF splitter, two lines of unequal length, and an RF mixer. The RF output of the UUT is divided by the splitter into two signals, unequally delayed. The required differential delay can be obtained by using two coaxial cables of, for example, 5 and 10 inches in length. The outputs of these delay lines are furnished to the two inputs of the RF mixer. For certain frequencies which may be identified by experiment, the mixer will produce a dc voltage near zero. The number of null frequencies can be increased by making the delay lines longer in absolute terms or by increasing the ratio between their lengths. If the output becomes frequency modulated, the mixer output voltage will change, and the voltage variation will be proportional to FM deviation. The polarity of the voltage change may be either directly or inversely related to the direction of frequency deviation. When voltage levels have been established for different frequencies, the mixer output can be monitored on an oscilloscope to provide a continuous display of FM deviation.

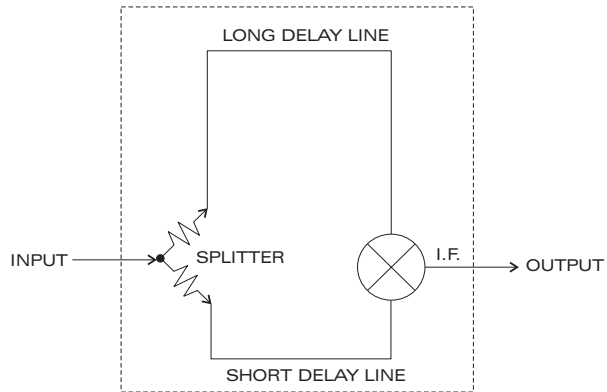


Figure 4-11: FM Test Fixture

1. Connect the FM test fixture to the RF OUT connector of the UUT. Monitor the mixer output with the oscilloscope (5 mV/div). Set the UUT to a null frequency (that is, at a frequency where the mixer output voltage is zero); +5 dBm out, no modulation.
2. Establish the voltages at 5 MHz above and 5 MHz below the null frequency. Adjust the oscilloscope gain and the UUT output power level (near +5 dBm) to place the null point at the center of the screen and the 5 MHz deviation points at 3 divisions above and 3 divisions below the null point.
3. Connect an external 100 kHz TRIANGLE source at $2 V_{p-p}$ to the FM MOD input. Verify that the waveform is six divisions peak to peak ± 0.6 divisions.
4. Change external signal to SIN WAVE at a 100 kHz rate, $2 V_{p-p}$ in 6 divisions (± 0.6). Verify that the waveform is peak to peak.
5. Adjust the UUT FM deviation for a six division peak to peak display. Vary the function generator from 10 Hz to 1 MHz and verify that the display remains between four and eight divisions peak to peak.

Series 50000B VXIbus Microwave Synthesizers

Series 50000B VXIbus Microwave Synthesizers Data Sheet (Page 1 of 4)

Serial Number:		NOTE: In the space provided for test results, record the measured value (if any). In the case of a function check or range check, write OK to indicate the unit under test meets specifications.	
Date:			
Tested By:			
Quality Assurance:			
Test	Section	Setting/Specification	Test Result
Frequency Range, Resolution, Accuracy	4.2.3	.01-2 GHz band (if installed) 10 MHz \pm 1 Hz \pm counter resolution	
	Step 2		
	Step 3	Maximum frequency \pm 1 Hz \pm counter resolution	
	Step 4	PLL test frequencies, \pm 1 Hz \pm counter resolution:	
		2000	
		3520	
		3620	
		3670	
		3700	
		3850	
		3880	
		11210	
		11220	
		11350	
		11360	
		11390	
		11400	
	11420		
	Step 5	1 Hz resolution test frequencies (use any frequency for >100 kHz digits)	
		XXXX.000000	
XXXX.111111			
XXXX.222222			
XXXX.444444			
XXXX.888888			
XXXX.999999			

Series 50000B VXIbus Microwave Synthesizers
Data Sheet
 (Page 2 of 4)

Serial Number:		NOTE: In the space provided for test results, record the measured value (if any). In the case of a function check or range check, write OK to indicate the unit under test meets specifications.
Date:		
Tested By:		
Quality Assurance:		

Spurious Signals Tests (Section 4.2.4)

Frequency	Harmonics		Non-Harmonics					
			<100 kHz		100 kHz <1 MHz		>1 MHz	
	Spec	Result	Spec	Result	Spec	Result	Spec	Result
411.226	<-40		<-40		<-50		<-60	
1333.288	<-40		<-40		<-50		<-60	
2409.976	<-50		<-40		<-50		<-60	
3536.171	<-50		<-40		<-50		<-60	
6869.565	<-50		<-40		<-50		<-60	
9182.433	<-50		<-40		<-50		<-60	
12317.392	N/A		<-40		<-50		<-60	
15421.056	N/A		<-40		<-50		<-60	
17361.522	N/A		<-40		<-50		<-60	

Test	Section	Setting, Specification	Test Result
Single Sideband Phase Noise (@ 10 kHz offset)	4.2.5	Test frequencies in MHz, specifications in dBc/Hz	
		411, <-75	
		1333, <-75	
		2409, <-77	
		3536, <-77	
		6869, <-77	
		9182, <-75	
		12317, <-72	
		15421, <-72	
		17361, <-72	

Series 50000B VXIbus Microwave Synthesizers

Series 50000B VXIbus Microwave Synthesizers Data Sheet (Page 3 of 4)

Serial Number:		NOTE: In the space provided for test results, record the measured value (if any). In the case of a function check or range check, write OK to indicate the unit under test meets specifications.	
Date:			
Tested By:			
Quality Assurance:			
Test	Section	Setting/Specification	Test Result
RF output power	4.2.6 step 1	See Specifications	
	step 2	level 0 dBm ± 2 dB over entire range	
	step 3	step attenuator test frequencies (GHz):	
		1.0	
		4.0	
		7.0	
		9.0	
		12.0	
		17.0	
Pulse Modulation Tests			
Frequency (GHz)	On/Off (Section 4.2.7)	Rise/Fall (Section 4.2.8)	Overshoot (Section 4.2.9)
1.0			
4.0			
7.0			
9.0			
17.0			
Specification:	(>80 dB)	(<25 ns)	(< ± 2 dB) Typical

Series 50000B VXIbus Microwave Synthesizers Data Sheet (Page 4 of 4)				
Serial Number:		NOTE: In the space provided for test results, record the measured value (if any). In the case of a function check or range check, write OK to indicate the unit under test meets specifications.		
Date:				
Tested By:				
Quality Assurance:				
Amplitude Modulation Tests (Section 4.2.10)				
Frequency (GHz)	Max. Depth	Ext% AM	Bandwidth	Distortion
1				
4				
7				
9				
12				
17				
Specification:	>82%	50% \pm 10%	\pm 3 dB	<10%
Frequency Modulation Tests (Section 4.2.11)				
Frequency (GHz)	Deviation		Bandwidth	
1				
4				
7				
9				
12				
17				
Specification:	5.4 - 6.6 div		4 - 8 div	

Maintenance

5.1 Introduction

5.1.1 Warranty

During the warranty period of the instrument, we recommend that you consult Giga-tronics or an authorized Giga-tronics representative before initiating any repair work. Operational problems can often be isolated to a replaceable module, for which a replacement can be ordered.

5.1.2 Safety Precautions

It may become necessary to access the interior of the instrument while power is on, in order to observe internal system operation. In this case, extender boards or cables (to extend the module outside of the mainframe), or the removal of the mainframe housing, will be necessary. Be certain to provide adequate cooling if the synthesizer module is removed from the VXI frame. A small table top fan blowing on the module will suffice.

Modules and circuits should not be disconnected or reconnected while power is on! Always power down the mainframe before making such changes.

CAUTION

This instrument contains MOS and CMOS devices; be sure to use appropriate anti-static procedures whenever it is necessary to handle them.

5.1.3 Preliminary Troubleshooting

If the instrument appears to be malfunctioning, three potential problem areas need to be examined before any other analysis of the problem is attempted:

- Verify that the modules are all properly seated in the appropriate mainframe slots, and have their address switches set correctly
- Verify that all required external signals are being received by the modules, including power supply inputs, reference frequencies, and bus inputs
- Be sure that the modules are receiving the appropriate commands over the bus. An apparent malfunction may be the result of incorrect commands or addressing

5.2 Failure Analysis

5.2.1 Defining the Malfunction

It is important to define the malfunction precisely, and to determine under what circumstances it occurs. If the problem is known to occur only in a particular operating mode, or in a particular area of the instrument's frequency range or level range, it may be easier to identify the circuit at fault.

Nine major areas of potential failure are discussed below, with reference to the troubleshooting notes included in Section 5.3 (e.g., see 5.3.1).

5.2.2 General Failure

The instrument does not function at all; commands sent to it over the bus have no effect.

Recommendations:

1. Check the power supplies (see 5.3.1).
2. Check the VXI slot zero system controller (see 5.3.2).
3. Check the Giga-tronics 52000B Control module (see 5.3.15).
4. Verify that the correct bus addresses and module positions are being used (see 5.3.21).
5. Verify that the correct remote commands are being used (see 5.3.22).
6. Verify that all modules are in the correct order (see 5.3.21).

5.2.3 Loss of RF Output

There is no measurable power present at the output connector regardless of the RF level setting; the front panel LEVEL indicator may or may not be lit.

Recommendations:

1. Check the power supplies (see 5.3.1).
2. Check the downconverter, if the instrument includes the range below 2 GHz (see 5.3.23).
3. Check the 10 dB step attenuator (see 5.3.3).
4. Check the filter select (see 5.3.4).
5. Check the YIG oscillator (see 5.3.5).
6. Verify that pulse modulation has not been activated inadvertently.

5.3 Troubleshooting Notes

5.3.1 Power Supplies

A variety of malfunctions can be caused by power supply problems. Because the system has many regulated supplies operating somewhat independently, it is possible for the failure of single supply to disable only a part of the system. Power supply voltages should be checked whenever there is a malfunction, even though the malfunction may seem too specialized to have such a cause.

The system takes its power supplies from the backplane of the VXI mainframe, through the P1 and P2 connectors.

The power supplies originate from the backplane of the VXI mainframe through connectors P1 and P2. From there, the supplies are converted down to lower voltages through a series of regulators located at the synthesizer's Power Supply (A 46). Bypass capacitors are located on the inputs and outputs of the regulators. The individual supplies are:

- +24 volts (drives relays in the 10 dB attenuator and is a source for +18 V and +15 V regulators on the top plate assembly). Test points: P21-8(A2) (check A2-C6 cap), and P10-6(A1) (check A1-C6 cap). Wire color: Yellow
- -24 volts (source for -18 V regulators on the top plate assembly). Test point: P21-7(A2). Wire color: Orange
- +12 volts (used by amplifiers, drivers, etc.). Secondary regulators on circuit boards convert the supply to a lower voltage where necessary. Test point: P10-3(A1). Wire color: White/Red
- -12 volts (source for the -5.2 V regulators on the top plate assembly). Secondary regulators on circuit boards convert the supply to a lower voltage where necessary. Test points: P21-5(A2) & P10-7(A1). Wire color: White/Green
- +18 volts #1 (used by amplifiers, drivers, etc.). Secondary regulators on the circuit boards convert the supply to a lower voltage where necessary. Test point: P21-1(A2). Wire color: Blue/Orange
- +18 volts #2 (source for heater voltage and tuning-coil current by the YIG oscillator. Test point: P10-1(A1). Wire color: Blue/Orange
- -18 volts (used by amplifiers, drivers, etc.). Secondary regulators on circuit boards convert it to a lower voltage where necessary. Test points: P21-2(A2) and P10-2(A1). Wire color: Violet/Orange

Check the input and output of the regulator for the faulty supply (the regulators are on the top plate assembly in the synthesizer module, and on the A1 PC board in other modules). If the input is absent or incorrect, check the mainframe supply (isolate the supply from the regulator, to determine whether the mainframe supply is being overloaded). Also, check the capacitors at the P1 and P2 connectors on the A1 and A2 PC boards in the modules.

If the mainframe supplies are normal, try removing the load and checking the output to see whether the problem is caused by an overload on the regulator (then identify and repair whatever is overloading the regulator). If the regulator is not being overloaded but continues to produce the wrong voltage, replace the regulator.

5.3.2 VXI Slot Zero System Controller

The slot zero system controller must be operating properly for the Giga-tronics synthesizer to operate properly. Most slot zero controllers contain a SYSTEM FAIL indicator; green usually indicates normal operation, and red normally indicates either a reset or a complete power-down and power-up again of the entire VXI mainframe is required.

It is important to verify that the slot zero controller is functioning properly before troubleshooting the synthesizer. Remove all of the VXI modules from the VXI bus to isolate the slot zero controller. If the SYSTEM FAIL light continues to indicate a failure during power-up, replace the slot zero controller.

5.3.3 10 dB Step Attenuator

The programmable attenuator is capable of reducing the amplitude of the RF output by as much as 90 dB. If the output is not at the desired power level, the cause may be that the attenuator is improperly set. Note that the attenuator is outside the leveling loop; therefore, the level control circuit cannot detect, or compensate for, attenuator errors.

The attenuator internal structure includes four programmable relays, which add or remove lossy elements rated in 10 dB multiples (10 dB, 20 dB, 30 dB, 30 dB) in whatever combination is necessary to achieve the desired total attenuation.

The relay drivers which select and deselect these elements are located on the Attenuator/Pulse Driver PC board (A4) in the Synthesizer module. Verify that the attenuator is receiving the appropriate drive signals; if not, investigate the drivers (on the circuit board which houses them) and the logic lines which control them.

5.3.4 Filter Select

The signal path through the 2-20 RF module (A201 in the Synthesizer module) is divided into a number of filter lines. The number of lines actually used depends upon the output bandwidth; the ranges of the individual filter lines (in GHz) are 2-3.2, 3.2-5.2, 5.2-8, 8-12 and 12-20. If the filter select control line for the active path is held in the off condition, the RF signal will be shut down.

The filter select control lines applied to the RF module have voltage levels of (roughly) -1 V for ON and +1 V for OFF. The signals originate on the Attenuator/Pulse Driver PC board (A4) in the Synthesizer module. If inappropriate drive signals are being received, investigate the driver circuits and their corresponding computer logic lines.

5.3.5 YIG Oscillator

All YIG oscillators require a +15 V power supply; some YIGs also require a -5 V power supply. The YIG must have current supplied to its tuning coil, within an appropriate range, in order to generate an RF output. If the tuning coil current is too high or too low, there will be no signal.

The easiest way to measure coil current is to read the voltage drop across the sense resistor. This is a large, high-wattage, metal-encased resistor, usually rated at 5 Ω or 7 Ω (depending on the oscillator used), mounted near the YIG. One end of the sense resistor is grounded, and the other end is connected through an NPN transistor (Q1) to the negative end of the YIG oscillator tuning coil. Q1 is controlled by the YIG Driver PC board (A3 in the Synthesizer module).

To determine the coil current, measure the voltage drop across the sense resistor, and divide the resistor's voltage drop by its resistance. Since the tuning sensitivity of the YIG oscillator is

approximately 20 MHz/mA, the appropriate coil current in Amps for a given frequency can be estimated by dividing the frequency (in GHz) by 20.

Coil-current values corresponding to frequencies outside the range of the oscillator will shut it down. If this situation exists, investigate the NPN transistor (Q1) and the YIG Driver circuit (A3).

5.3.6 Leveler

The signal path through the 2-20 RF module (A201 in the Synthesizer module) includes a voltage controlled attenuator circuit, or leveler. The Level/RF PC board (A2 in the Synthesizer module) produces a control output which drives the leveler input pin on the outside of the 2-20 RF module. The leveler increases attenuation as the input goes more positive and reduces attenuation as the input goes more negative. The sensitivity of the leveler to the control input varies substantially from one module to another; however, the voltage swing measured at the leveler input pin is (very roughly) from -14 V to +2 V.

When the output level is incorrect, the leveler input may be obviously wrong in a way which suggests the cause of the problem.

1. If output power is too low, and the leveler input is at the positive rail (maximum attenuation), the level control circuit is reducing the output power by sending the wrong control signal.
2. If output power is too low, and the leveler input is at the negative rail (minimum attenuation), the level control circuit is striving unsuccessfully to compensate for power loss occurring somewhere in the RF path.
3. If output power is too high, and the leveler input is at the positive rail (maximum attenuation), the leveler circuit itself is faulty.
4. If output power is too high and the leveler input is at the negative rail (minimum attenuation), the level control circuit is increasing output power by sending the wrong control signal.
5. If the level control voltage is between the extremes of its range, but the output level is incorrect, the fault is probably in the level control circuit (A2).

A failure of the leveler, or other circuits within the 2-20 RF module, is unlikely, but can be caused by excessive reverse power applied at the synthesizer's RF output connector.

5.3.7 Level Detector

The level control circuit requires feedback from the RF path in order to monitor and adjust output power. This feedback is provided by a negative-output diode detector, driven by a signal coupled from the RF output path. The internal detector is mounted directly on the level coupler output of the 2-20 module (A201 in the Synthesizer module).

A failure of the level detector is unlikely; however, it is important to verify that the detector's signal is being received by the Level/RF PC board (A2 in the Synthesizer module). An easy way to investigate this is to disconnect and reconnect the detector cable, and observe any resulting level changes.

5.3.8 Level Control Circuit

The level control circuit, which is contained in the Level/RF PC board (A2 in the Synthesizer module), consists of a loop amplifier which balances a variable input (feedback from the level detector) against a reference signal. The reference signal consists of a combination of two inputs: the leveling reference input which is programmed by the system computer, and a temperature compensation signal from the YIG Driver/Temp Comp PC board (A3 in the Synthesizer module). The level control circuit adjusts output power by using its output to drive the leveler in the 2-20 RF module (A201 in the Synthesizer module). The leveler is driven in whichever direction will equalize the reference and variable inputs to the loop amplifier. When the control output to the leveler is within its control range, the RF output is considered to be leveled, and the indicator on the front panel will remain lit.

- 1. If it appears that the level control circuit is sending the wrong control signal to the leveler (see 5.3.6), it is likely that the level control circuit is receiving a bad input or is incorrectly calibrated.
- 2. Check all inputs and control signals to the level control circuit, including the detector input, the temperature compensation input, and the data lines to the digital-to-analog converter. Experiment by breaking the leveling loop (disconnect the detector cable) and observing the resulting changes.
- 3. Try to correct the problem by recalibrating the level control circuit (see Chapter 4).
- 4. Be sure that the instrument is using the correct level characterization data for the current configuration of VXI modules. For example, if the system was characterized with a downconverter module installed, be sure that the downconverter module is still installed and that all RF cabling is securely attached.
- 5. If possible, replace the level control circuit with a spare.

5.3.9 Lock Indicators for PLL Circuits

Each four phase lock loop circuits has an UNLOCK indicator, an LED which is lit when the loop is unlocked (the reverse of the front panel LOCK indicator).

If the RF output frequency is unlocked, begin by determining which loop is unlocked. If two or more loops are unlocked, it is possible that only one PLL circuit is faulty, and is disabling subsequent loops which use its output as a reference. The hierarchy of PLL circuits, in terms of this dependency, is outlined below as a set of two branches which begin with the 110 MHz PLL and end with the Output PLL. If two or more PLLs are unlocked, begin by investigating the one which is nearest the top of Table 5-1:

Table 5-1: PLL Circuit Hierarchy

Reference Branch	Variable Branch
110 MHz PLL (Control module, A101)	110 MHz PLL (Control module, A101)
80 MHz PLL (Synthesizer module, A1)	300 MHz PLL (Synthesizer module, A2)
Output PLL (Synthesizer module, A2)	Output PLL (Synthesizer module, A2)

5.3.10 Output Phase Lock Loop

The Output PLL is located on the A2 PC board in the Synthesizer module. Check for appropriate inputs from the Divide-by-2 circuit, which is located on the same board, and the DDS circuit, which is located on the A1 PC board.

1. The output to the YIG oscillator FM coil goes more positive to reduce frequency, more negative to increase frequency; verify that the Output PLL is not driving the YIG in the wrong direction.
2. Verify that the PLL output is reaching the YIG FM coil.
3. If possible, replace the circuit board with a spare.

5.3.11 Divide-by-2 Circuit

This circuit is located on the A2 PC board in the Synthesizer module.

1. Verify that the 6-40 MHz IF input is being received from the 300 MHz Oscillator circuit (A104 in the Synthesizer module).
2. Verify that the IF input to the divider is being correctly divided, and furnished to the phase detector input of the Output PLL circuit.
3. If possible, replace the circuit board with a spare.

5.3.12 300 MHz Oscillator

The 300 MHz Oscillator PC board (A104) is encased in an aluminum housing mounted on the synthesizer chassis beneath the 2-20 RF module. The location of this circuit makes it difficult to access. The most that can normally be done to investigate it in the field is to verify that it is receiving the required inputs from the RF coupler and the 300 MHz PLL (see A2 of the Synthesizer module), and that it is producing the IF input required by the Divide-by-2 circuit (also on A2 of the Synthesizer module).

5.3.13 300 MHz Phase Lock Loop

The 300 MHz PLL is located on the Level/RF PC board (A2 of the Synthesizer module).

1. Verify that the necessary inputs are being received: 330 MHz from the 330 MHz buffer, 10 MHz from the 10 MHz buffer, feedback from the 300 MHz oscillator (A104 of the Synthesizer module), and control signals from the local bus.
2. Verify that the output tuning voltage is present and is reaching the 300 MHz oscillator.
3. If possible, replace the circuit board with a spare.

5.3.14 YIG Oscillator Driver

The YIG driver circuit is located on the YIG Driver/Temp Comp PC board (A3 of the Synthesizer module).

1. If the YIG driver is coarse-tuning the YIG oscillator to the wrong frequency, the error may be too large for the output PLL circuit to correct. This problem sometimes occurs after incorrect adjustment of the MIN and MAX pots, in which case the output loop may lock at some frequencies but not others. If the synthesizer develops phase lock problems following calibration of the YIG driver, try repeating the calibration (use the procedure in Chapter 4).
2. If the driver calibration is not the cause of the problem, attempts to adjust it may only aggravate the condition. Therefore, it is a good idea to determine first whether or not the driver output is approximately correct for the requested output frequency. As described in 5.3.5, the oscillator tuning coil has a sensitivity of 20 MHz/mA. The NPN transistor which controls the coil current is driven at its base by the control output signal of the YIG driver. Because of large variations in coil impedance, it is not possible to specify a correct voltage. However, it should be a positive voltage increasing with frequency at a rate of roughly 650 mV/GHz. A more exact idea of the coil current can be calculated by measuring the voltage drop across the sense resistor (see 5.3.5).
3. If the driver output seems to be substantially wrong, the cause could be incorrect control data to the driver's digital to analog converter, as well as faulty calibration.
4. If possible, replace the circuit with a spare.

5.3.15 Model 52000B Control module

The Control module contains the VXI Interface Control PCA and IT Daughter Card (the 110 MHz Assembly and the 10 MHz Master Reference are also housed within the Control module).

The VXI/Interface Control PCA and IT Daughter Card provide the VXI Bus interface, the decoding circuitry and interface chips used for communicating on the Local Bus, and the power supply regulators for the modules and circuits located off the PCA.

1. Check the power supplies from the VXI mainframe to the +18 V, -18 V, +5 V, & -5 V regulators. Check the computer +5 V supply at U1A1 pin C20.
2. If possible, replace the PC board with a spare.

5.3.16 110 MHz Assembly (A101)

The 110 MHz assembly supplies timebase-derived reference frequencies to the synthesizer. The 110 MHz Oscillator/Multiplier circuit board and the 110 MHz PLL are combined and encased in a aluminum housing mounted alongside the VXI/Interface Control Board.

110 MHz Oscillator/Multiplier

Verify that the tuning input is being received from the 110 MHz PLL. Also, verify that the tripler output (330 MHz) is correct.

110 MHz PLL

Verify that the 10 MHz input is being received from the master reference. Verify that the 110 MHz feedback input is being received from the 110 MHz oscillator. If possible, replace the PLL circuit with a spare.

5.3.17 10 MHz Master Reference (A2)

The 10 MHz internal timebase TCXO is located below the 110 MHz assembly; the 10 MHz input/output circuit is located on the 110 MHz PLL circuit board.

1. Verify that the signals from the internal timebase and the external timebase (if any), are being received by the 10 MHz input/output circuit.
2. Verify that the 10 MHz signal from the input/output circuit is reaching the various PLL circuits which require it.

5.3.18 DDS Circuit

The DDS circuit is located on PC board A1 in the Synthesizer module.

1. Verify that the 80 MHz input is being received from the 80 MHz PLL (located on the same circuit board).
2. Verify that the 3-20 MHz output is reaching the reference input of the Output PLL (located on PC board A2 in the Synthesizer module).
3. If possible, replace the circuit with a spare.

5.3.19 80 MHz Phase Lock Loop

The 80 MHz PLL is located on PC board A1 in the Synthesizer module.

1. Verify that the 10 MHz input is being received from the 10 MHz Buffer Assembly (A101 in the Synthesizer module).
2. Verify that the 80 MHz output is reaching the Direct Digital Synthesis circuit.
3. If possible, replace the circuit with a spare.

5.3.20 FM Driver

The FM Driver circuit is located on the regulator PC board (mounted near the YIG).

Verify that the output signal is correct at the two PIN connector. The output goes more negative in order to increase the frequency (see Section 5.3.10).

5.3.21 Local Bus Address

There is a position requirement when installing modules into a VXI mainframe. The Model 52000B Control module must be at the left (as viewed from the front). The Synthesizer module is placed immediately to the right of the Control module; any other modules must be placed contiguously to the right of the Synthesizer module.

DIP switches are externally accessible on each module. The switches on the Control module are for VXIbus Logical Addressing; the switches can be set to a specific address, or set to the Dynamic Configuration Mode (address FF) by placing all the switches in the ON position. Other modules use these switches to represent Local Bus addresses 0 through 7.

1. Use native Syntax command LLA (list local addresses) to verify that the address assigned to each module corresponds to the address switch setting.
2. If a module is not recognized on the local bus, make sure that it is properly seated in the mainframe. Investigate the decode circuitry on the Address/Decode circuit for that module.

5.3.22 Commands

Chapter 2 includes a full description of the syntax and commands appropriate to the operation of the Series 50000B instruments. Be sure that any commands issued to the instrument conform to the guidelines in that description.

5.3.23 Downconverter

During operation in the downconverter range, a switch diverts the YIG-generated output of the RF module to a mixer, where it is combined with the fixed 7.92 GHz output of a Dielectric Resonant Oscillator. This downconverter mixer generates an intermediate frequency which has a range of .01 to 2 GHz; the IF is equal to the difference between the YIG frequency and 7.92 GHz.

Measure proper voltage on the regulators on the Address/Decode board. Check the Mixer/Amp and DRO supplies for +15 V. If the Downconverter Switch is set to the wrong position, the RF output path will be blocked.

Verify that the control lines from the Address/Decode PCA (A1) are within 0.5 V of the test points in Table 5-2:

Table 5-2: Regulator Voltage Points

A1 Test Point	<2 GHz	>2 GHz
E17	-10 V	+15 V
E18	+0.9 V	-5.6 V
E19	+15 V	0 V
E6	+2 V	0 V
U10-12	0 V	+5 V



Options

A.1 Introduction

This appendix describes the options that are available for use with the Series 50000B VXIbus Microwave Synthesizers.

A.2 Option 26: 10 dB Step Attenuator

If Option 26 is installed, a programmable 10 dB step attenuator is placed in the Synthesizer module or the Downconverter module. The attenuator makes it possible to extend the instrument output power range downward to -90 dBm.

The exact configuration of the option is determined by customer preference.

Parts List: 29850 - STEP ATTENUATOR, Rev. E

Item	Part Number	Qty	Cage	Mfr's Part Number	Description
1	MP90-02604	1	26840	33326K H89/104	0-90DB 26 GHZ PGM ATTEN
2	MPXX-00003	1	26840	11764C	8 ATTEN RIBBON CABLE
3	WCAS-18106	1	0DJ29	P-3636-601-5206	6" 18 GHz SEMI-FLEX COAX
4	30691	1	58900	30691	ATTENUATOR MOUNT
5	410BF02500	-1	58900	410BF02500	VXI ATTENUATOR MOUNT
101	HMPP-03010	2	56563	M3X10 PP SS	3MM X 10MM PAN
102	HWSS-40300	6	58900	HWSS-40300	#4 X 3/16 SPLIT LOCK
103	HMFP-03008	2	58900	HMFP-03008	3MM X 8MM FLAT
104	HWFS-40300	4	7U905	NAS620-C3	#4 X 3/16 FLAT WASHER
105	HBPP-44005	2	26233	NS137CR440R5	4-40 X 5/16 PAN

